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**LONG-TERM YIELD ANALYSIS  
OF THE  
LOWER GULCHES AND DRYDOCK GULCH RESERVOIR  
TRIBUTARY TO THE BIG RIVER  
FOR A  
WATER SUPPLY  
FOR THE  
TOWN OF MENDOCINO**

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## **Introduction**

This report sets forth an investigation of,

(1) the long-term yield of the combined flow of the Lower Gulches (Thicket Draw, Beans Gulch, Waterspout Gulch, and Nelsons Gulch) for the 44-year period 1948 through 1992, and

(2) the long-term combined yield of the Lower Gulches and Drydock Gulch under various alternatives reflecting the height and volume of storage within Drydock Gulch.

Analysis of yield reflect streamflow measurements taken during the summer of 1991 (Lawrence & Associates, July 25, 1991) and 1992. In addition to streamflow measurements, a drawdown test was conducted in late October, 1992 on Drydock Gulch to estimate baseflow.

Of particular importance to this study was to estimate the minimum flow that would occur during the 2-year critical-dry period 1975-76 and 1976-77. A previous study (Lawrence & Associates, July 25, 1991) showed the Big River near the Mendocino Woodlands had gone dry during the summer of 1977. The drainages below and including Drydock Gulch studied for the current analysis, however, drain terrace deposits that contain carry-over storage from one year to the next.

## **Findings**

1. During the 2-year critical-dry period 1975-77, when 2-year cumulative precipitation was 59 percent of normal, the minimum summer yield from the Lower Gulches and Drydock Gulch, based on reservoir capacity of Drydock Gulch, is:

Water Year	Reservoir capacity (AF)/depth (ft)			
	40/13.6	25/9.2	15/6.3	7.2/4 (present condition)
			(GPM)	
1975-76	234	211	196	184
1976-77	171	156	140	124

2. During the critical-dry year 1990-91, when precipitation was 63 percent of normal (the 2nd driest year to 1976-77), the minimum summer yield from the Lower Gulches and Drydock Gulch, based on reservoir capacity of Drydock Gulch, is:

Water Year	Reservoir capacity (AF)/depth (ft)			
	40/13.6	25/9.2	15/6.3	7.2/4 (present condition)
			(GPM)	
1990-91	210	188	172	161
1991-92	253	230	215	203

3. With the exception of the above years, minimum summer yield from the Lower Gulches and Drydock Gulch, based on reservoir capacity of Drydock Gulch, equals or exceeds the following yields:

Reservoir capacity (AF)/depth (ft)			
40/13.6	25/9.2	15/6.3	7.2/4 (present condition)
		(GPM)	
237	214	199	188

4. Depending on the approach, the analysis of the drawdown test on Drydock Gulch gave varying results of baseflow because approximately 2 inches of rainfall occurred during the test. Because of this, a very conservative estimate of baseflow was estimated and used in the yield analysis.

5. Under existing conditions, the Drydock Gulch pond has a maximum depth of 4 feet, a capacity of 7.2 AF (acre-feet), and a surface area of about 3.2 acres, when the water level is at the invert of the culvert which drains the pond to the Big River estuary.

6. Raising the water level of the Drydock Gulch pond by about 6 feet above the culvert inlet would leave the water level about 4 feet below the logging road that dams the pond between the gulch and the Big River estuary.

### **Conclusions**

*Added numbers*  
With the combined flow of the Lower Gulches, a dam constructed across Drydock Gulch that would contain about 25 AF at a maximum depth of about 9 feet, would provide a minimum summer yield of about 190 gpm or greater for every year of the 44-year record, except for one year, when the yield would be about 156 gpm.

### **Analysis**

#### **Discharge of Lower Gulches period 1991 and 1992**

The analysis of the Lower Gulches, which include Thicket Draw, Beans Gulch, Waterspout Gulch, and Nelsons Gulch, during the 2-year period 1991 and 1992 is based on measured and estimated flows. A description of the drainages together with field observations of flow and quality are contained in the "Big River Study" (Lawrence & Associates, July 25, 1991).

The "Big River Study" contains field measurements made during the summer of 1991. Additional flow measurements were made on the Lower Gulches during the summer of 1992.

The determination of daily and annual flows of the Lower Gulches for the 44-year long-term period is based on two years when precipitation was below normal for both years. One of the years, 1990-91, was the driest year of record next to the year 1976-77. Because of this dry condition, the estimate of flows herein during a critical dry period (1974-77) is somewhat verified with field observations taken during a similar dry period, and therefore can be treated with some confidence.

As a first step in estimating the historical record of discharge, daily flows for the Lower Gulches were synthesized from stream measurements taken between June 14, 1991 and October 28, 1992, as shown on Table 1, and Figures 1 and 2 for the years 1990-91 and 1991-92, respectively.

Daily flows for each gulch were determined for each year by straight-line interpretation between the days having observed and estimated flows. The daily flows were then summed to give a total flow for the Lower Gulches for each year for the period June 14 through October 28, for both years 1990-91 and 1991-92.

For each day of the period June 14 through October 28, the percent of the average-daily flow to the daily flow was calculated for each year. The average values of the daily percentages for the two years were calculated and plotted, as shown on Figure 3. From this curve a trend curve was drawn to complete the remainder of the year, as shown.

The location of the trend curve between October 29 and June 13 is based on the following criteria/assumptions:

1. The maximum day occurs approximately during the middle of April, as reflected by the shape of the baseflow curves shown on Figures 4 through 7.
2. The flow on the maximum day is only greater than the observed flow on June 14 within reasonable limits of drawing a "smooth" curve through the data points.



3. The flow observed on October 28 represents the lowest flow of the year.

4. The percentage flow occurring on October 1 at the beginning of the year is the same as the percentage flow occurring at the end of the year. (When the actual daily flow is calculated this would not be absolutely correct, as it would require the preceding year to have the same average discharge between June 14 and October 28 as the year being calculated.)

With the percentage trend-curve completed for the whole year, as shown on Figure 3, the daily flow was calculated for the years 1990-91 and 1991-92 by multiplying the daily percentages by the average summer flow. For 1990-91 and 1991-92 the average summer flow was 140 gpm and 184 gpm, respectively. The calculated daily flows for each year are shown on Figure 8.

#### **44-year-period annual discharge of the Lower Gulches**

To calculate the annual discharge of the Lower Gulches a relationship between annual precipitation and gulch flow for the years 1990-91 and 1991-92 was established, as shown on Figure 9.

The intercept of the curve on the y-axis indicates there would be approximately 30 gpm of average summer discharge even if the preceding winter had zero rainfall. This can be believed, because it would be expected that the terrace deposits would not completely drain even with an absolutely dry winter.

The equation for the curve shown on Figure 9 was applied to each year of the 44-year periods to arrive at an annual yield of the Lower Gulches, as shown on Table 2.

#### **Baseflow of Drydock Gulch**

A drawdown test to determine baseflow was conducted on the pond behind the logging road within the Drydock Gulch drainage. The test was interrupted by rainfall and the calculated baseflow varies based on the time interval

evaluated during the test. The estimated baseflow is shown on Table 3, and varies between about 18 gpm and 90 gpm. The three time intervals evaluated occurred under the following conditions:

(1) Pretest - Water levels were rising in the pond prior to the start of the pumping test, as shown on Figure 10. The inflow of 90 gpm was calculated based on the time interval of 85 minutes and the volume (pond area times rise in level) of water entering the pond.

(2) Drawdown w/o rain - The early part of the drawdown test before rain began, as shown on Figure 11, gave a calculated baseflow of about 18 gpm. Calculated over a period of 3220 minutes, the inflow was calculated as the difference in the volume of water pumped and the change in pond storage.

(3) Drawdown plus recovery - Calculated baseflow during both the drawdown and the recovery period, as shown on Figure 11, gave an estimated inflow of about 49 gpm. During this 4550-minute period, approximately 2 inches of rainfall occurred, as measured in a 5-gallon bucket placed in the open. Baseflow was calculated as difference between volume pumped, volume of direct precipitation, and change in storage.

For the above three intervals of calculation, evaporation was deducted as an outflow. Estimates of evaporation were based on temperature measured during the test, as shown on Figure 12, and the correlation between evaporation and temperature, as shown on Figure 13.

The essence of this evaluation is to be conservative, and not to over estimate the amount of supply which is available. Using this criteria, the lowest calculated baseflow of 17.8 gpm was estimated to be the flow occurring on October 27 and 28, 1992.

Using the daily-percentages-of-summer-flow values, as shown on Figure 3, it can be seen that the October 27/28 value is about 73 percent of the average summer flow. Dividing 17.8 gpm by 0.73 gives an average summer discharge of about 24.4 gpm, for the period June 14 through October 28.

To determine the annual-average summer baseflow for Drydock Gulch, the assumption was made that the flow to Drydock Gulch was in proportion to the Lower Gulches. Using the ratio of the annual discharge for the Lower Gulches to the 1991-92-year discharge from the Lower Gulches, the baseflow to Drydock Gulch was calculated for the critical period 1974-79 and 1990-91, as shown on Table 4.

Using the average-annual summer flows, the daily baseflows for Drydock Gulch were calculated using the daily percentages shown on Figure 3, and the daily baseflows were plotted as shown on Figure 14, for the 4-year modeling-period, 1974-78.

As discussed previously, the daily percentages of flow shown on Figure 3 reflect the year beginning and ending with the same flow. This would rarely be the case because the average summer baseflow is dependent on the magnitude of precipitation occurring during the previous winter.

For the above reason, the ending and beginning of each year was connected with a trend curve for the 4-year-modeling period, as shown on Figure 14. The plot of rainfall shown on the figure was used as a guide in determining if the recession curve at the end of a year continued downward or started upward.

### **Surface flow to Drydock Gulch**

Surface runoff to Drydock Gulch during the 4-year modeling period 1974-78 was based on the daily unit runoff observed for the Navarro River. Unit runoff in cfs/square mile was multiplied by the Drydock drainage area of 0.5657 square miles to estimate the daily surface inflow to the gulch.

Prior to estimating the unit runoff from the Navarro River watershed, the daily flows for each of the four years were "scalped." That is, the surface-runoff portion of the total daily flow was separated from the "baseflow." Baseflow for Drydock was estimated separately. Scalping of the daily flows for the four years 1974-78 is shown on Figures 4 through 7 and 15 through 18.

Unit runoff was calculated by subtracting the daily scalped flow from the daily flow and dividing by the drainage area of the Navarro River above the stream gage.

### **Evaporation**

Evaporation correlated with maximum daily temperature was developed for use in the 4-year modeling period 1974-78. The line equation relating evaporation to temperature is shown on Figure 13, and was developed from four stations of record, as shown on Figures 19 through 22.

### **Area-depth-capacity curves for Drydock Gulch pond**

Area-depth-capacity curves for Drydock Gulch pond were developed for use in the 4-year modeling period 1974-78, as shown on Figures 23 and 24. The curves were developed from a depth-and-area survey conducted on the pond on October 26, 1992. Depth contours drawn from survey data points are shown on Plate II.

### **4-year modeling period 1974-75 through 1977-78**

The 4-year modeling period 1974-75 through 1977-78 was selected to evaluate the discharge that would occur during the driest 2-year period of record, 1975-76 through 1976-77. For these two years the cumulative precipitation was 59 percent of normal, as shown on the cumulative-deviation-from-the-mean curve, Figure 25, and on Table 5. Annual precipitation is shown graphically on Figure 26.

The model used is a computer-simulation model using daily time-steps. The model reflects an operation study of Drydock Gulch under various conditions of reservoir size, and considers items of evaporation, direct precipitation, surface runoff, baseflow, and yield. The model was combined with the daily estimated discharge from the Lower Gulches to determined a combined discharge.

Four reservoir sizes were selected for analysis:

7.2 AF capacity, maximum depth 4 feet (existing condition)						
15 AF	"	"	"	6.3 feet (alternative)		
25 AF	"	"	"	9.2 "	"	"
40 AF	"	"	"	13.6 "	"	"

Prior to running the model, the daily discharge from the Lower Gulches had to be evaluated for the 4-year period. As discussed previously, the daily percentages of flow shown on Figure 3 reflect the year beginning and ending with the same flow. This would rarely be the case, because the average summer discharge is dependent on the magnitude of precipitation occurring during the previous winter.

For the above reason, the ending and beginning of each year was connected with a trend curve for the 4-year-modeling period, as shown on Figure 27. The plot of rainfall shown on the figure was used as a guide in determining if the recession curve at the end of a year continued downward or started upward.

For each of the reservoir-size alternatives listed above, there is a variable daily yield from the reservoir, that when combined with the yield from the Lower Gulches, results in a constant daily yield. For example, Figure 28 shows the combined yield of Drydock and the Lower Gulches for a reservoir having a capacity of 40 AF. The minimum yield is 171 gpm, and it occurs throughout each day of 1976-77. As shown on the graph, the yield is a combination of water from storage and discharge of the Lower Gulches.

Looking at the year 1975-76 on Figure 28, the minimum yield is also 171 gpm, but the maximum yield is about 250 gpm. The maximum yield being derived from the Lower Gulches and none from the Drydock Reservoir.

For the 40-AF reservoir alternative, the actual water level in the reservoir during the 4-year modeling period would fluctuate as shown on Figure 29. Note the reservoir spills during the winter from storm runoff every year but the critical dry year, 1976-77. During the summer and fall of 1977 the

reservoir level is dropped to less than one foot in the process of drawing water out of storage.

The daily draw (or yield) on the Drydock reservoir during the 4-year modeling period is shown on Figure 30. Looking at the year 1976-77 and the few months before and after, beginning in September the draw increases throughout the fall, decreases during the winter, and increase during the summer and fall.

In other words, the draw when added to the discharge of the Lower Gulches, as shown on Figure 28, is just enough to provide a constant combined discharge. The draw is calculated to just deplete the water-in-storage before the next winter storm fills the reservoir and/or discharge from the Lower Gulches increases from precipitation.

Under present conditions at Drydock Gulch (7.2 AF of storage, 4-ft maximum depth), the pond would support a minimum of about 124 gpm (combined Drydock plus the Lower Gulches) during part of the critical dry year 1976-77, as shown on Figure 31; the maximum flow for the year would come from discharge from the Lower Gulches. Reservoir water levels and yield calculated during the 4-year modeling period are shown on Figures 32 and 33, respectively.

For the 15-AF, 6-ft-depth reservoir alternative, the combined yield of Drydock and the Lower Gulches, the reservoir water levels, and the yield, are shown on Figures 34, 35, and 36, respectively.

For the 25-AF, 9-ft-depth reservoir alternative, the combined yield of Drydock and the Lower Gulches, the reservoir water levels, and the yield, are shown on Figures 37, 38, and 39, respectively.

The relationships between reservoir yield versus depth and capacity are plotted on Figure 40. The curves can be used to estimate the minimum yield that would have occurred during the critical dry year 1976-77 under any combination of reservoir depth and capacity.

## Long-term yield of Drydock Gulch and the Lower Gulches

The long-term minimum yield of Drydock and the Lower Gulches was estimated for the 44-year period of precipitation October 1, 1948 through September 30, 1992 for the summer period June 1 through November 1, for the four reservoir alternatives:

7.2 AF	capacity,	maximum	depth	4 feet	(existing	condition)
15 AF	"	"	"	6.3 feet	(alternative)	
25 AF	"	"	"	9.2 "	"	"
40 AF	"	"	"	13.6 "	"	"

The long-term minimum summer yield of the combined flow from Drydock Gulch and the Lower Gulches was estimated using relationships developed between combined yield during the 4-year modeling period and precipitation, reservoir storage, and yield from the Lower Gulches and precipitation.

Results of the annual combined-yield analysis are shown on Table 6, and Figures 41 through 44 for the four reservoir alternatives, 7.2 AF, 15 AF, 25 AF, and 40 AF, respectively.

The evaluation process took the following steps:

1. For the 4-year period 1974-78, the daily flow on June 1 and November 1 of the Lower Gulches was read from the model output, and as reflected on Figure 14. For the years 1990-91 and 1991-92 the flow on these dates was determined from estimated data, as shown on Figure 9.
2. For each of the above 6 years, the average of the two flows occurring on June 1 and November 1 was calculated, and is considered to be the average summer flow.
3. The average-daily flow from reservoir storage alone was calculated for a 150-day period (June 1 through November 1) for each of the reservoir alternatives:

Capacity, AF	Storage yield, GPM
7.2	10.86
15	22.63
25	37.71
40	60.34

4. The storage yield for each of the reservoir alternatives was then added to the average summer discharge of the Lower Gulches, as calculated in Step 2.

5. The result calculated in Step 4 was then compared to the results obtained by the model study for the year 1976-77, it being the driest year of record, as shown below:

Drydock + Lower Gulches				
Method	Reservoir Storage, AF			
Calculated	7.2	15	25	40
Model	124	140	156	171
Annual method	133.99	145.76	160.84	183.47
Difference	9.99	5.76	4.84	12.47

Average difference = 8.26

For each of the reservoir alternatives, the values above show the minimum sustained yield for the year 1976-77 was, on the average, about 8.26 gpm less than the method used to calculate the average summer discharge.



6. The above difference of 8.26 gpm was subtracted from the combined flow of Drydock storage and the Lower Gulches calculated in Step 4, and plotted versus precipitation, as shown on Figure 45.

7. The plotted points shown on Figure 45 for each of the reservoir alternatives had a regression analysis to determine the equation of the best-fit curve through the points.

8. Using annual precipitation, the line equations shown on Figure 45 were used to calculate the minimum summer discharge that would occur annually for the 44-year period 1948-92, as shown on Table 6.

### **Drydock Gulch pond survey and drawdown test**

#### **Bottom survey**

On October 26, 1992 a survey of the depth of Drydock Gulch pond was conducted using a theodolite and EDM. Rod locations within the pond were held from a rubber dinghy, and angle/distance shots were made from one setup on the ground at the southeast corner of the pond.

Approximately 50 shots were made of the pond bottom and shoreline, and are plotted on Plate II. From these points, contours were constructed on the bottom of the pond and used for calculating area-depth-capacity curves, as shown on Figures 23 and 24.

It was noted while rowing the dinghy about that the pond has a number of submerged logs and fallen trees.

#### **Drawdown test**

Beginning at 1130 on October 27, 1992 a constant drawdown test was conducted for approximately 54 hours, and a recovery test for about 22 hours. Purpose of the test was to determine baseflow to the gulch.

Average pumping rate was 115.23 gpm. Drawdown in the pond was measured using a pressure transducer and data logger, as shown on Figures 10 and 11. Discharge from the pond was to the Big River estuary through the culvert underlying the logging road at the south end of the pond.

During the drawdown test, the air temperature, and the water temperature and conductivity of the pond were monitored continuously, as shown on Figure 12.

During the drawdown and recovery tests there was approximately 2 inches of rainfall. Rain began about 1730 on October 28, 1992, but did not become heavy until about midnight. As shown on Figure 12, while still pumping, recovery of the pond level began about midnight from rainfall. Rainfall was measured in a 5-gallon bucket set on the ground away from any trees.

### **Reference**

Lawrence & Associates, *Water resource inventory of the Big River drainage and vicinity for a water supply for the Town of Mendocino*, July 25, 1991.

Table 1  
Observed and Estimated Gulch Flow During Summers 1991 and 1992

Date	Thicket	Beans	Waterspout	Nelsons	Total
			(GPM)		
6/14/91	23 <sup>*a</sup>	37.78 <sup>*</sup>	43.18 <sup>*</sup>	97.20 <sup>*</sup>	201.16
7/8/92	16 <sup>*b</sup>	29.3 <sup>b</sup>	36.5 <sup>b</sup>	86.5 <sup>b</sup>	168.30
7/12/91	15 <sup>*a</sup>	28.35 <sup>*</sup>	35.44 <sup>*</sup>	85.05 <sup>*</sup>	163.84
10/14/91	10.72 <sup>c</sup>	15.14 <sup>c</sup>	23.33 <sup>f</sup>	53.90 <sup>g</sup>	103.09
10/28/91	10.72 <sup>d</sup>	15.14 <sup>d</sup>	23.33 <sup>d</sup>	53.90 <sup>d</sup>	103.09
6/14/92	32.17 <sup>h</sup>	49.91 <sup>i</sup>	58.67 <sup>j</sup>	121.73 <sup>k</sup>	262.48
7/8/92	22.39 <sup>*</sup>	38.71 <sup>*</sup>	49.59 <sup>*</sup>	108.33 <sup>*</sup>	219.02
10/14/92	15.00 <sup>*</sup>	20.00 <sup>*</sup>	31.67 <sup>*</sup>	67.50 <sup>n</sup>	134.17
10/28/92	15.96 <sup>*</sup>	20.00 <sup>*</sup>	30.69 <sup>*</sup>	67.50 <sup>o</sup>	134.15

Note reference:

- \* Unless otherwise noted, measured in the field with a 5-gallon bucket and stop watch.
- a Visual estimation; not able to measure directly.
- b Straight-line interpretation between measurements 6/14/91 and 7/12/91.
- c 10/14/92 Thicket flow times ratio of flow 7/8/91 to 7/8/92 ( $16/22.39 = 0.715$ ;  $15 \times 0.715 = 10.72$ ).
- d Assumed to be same as 10/14/91.
- e 10/14/92 Beans flow times ratio of flow 7/8/91 to 7/8/92 ( $29.3/38.71 = 0.757$ ;  $20 \times 0.757 = 15.14$ ).
- f 10/14/92 Waterspout flow times average of ratios calculated in Notes "c" and "e" above ( $(0.715 + 0.757)/2 = 0.736$ ;  $31.7 \times 0.736 = 23.33$ ).
- g 10/14/91 Waterspout flow times ratio of 2.31 calculated as the average ratio of 6/14/91 and 92 and 7/8/91 and 92 flows of Nelson to Waterspout ( $(97.2/43.18 + 86.5/36.5)/2 = 2.31$ ;  $2.31 \times 23.33 = 53.90$ ).
- h 6/14/91 Thicket flow divided by a ratio of 0.715 ( $23/0.715 = 32.17$ ); see Note "c" above.
- i 6/14/91 Beans flow divided by a ratio of 0.757 ( $37.78/0.757 = 49.91$ ); see Note "e" above.
- j 6/14/91 Waterspout divided by a ratio of 0.736 ( $43.18/0.736 = 58.67$ ); see Note "f" above.
- k 6/14/91 Nelsons flow divided by a ratio of 0.7985 ( $97.2/0.7985 = 121.73$ ); ratio determined from ratio between Nelsons flow on 10/14/91 and 10/14/92 ( $53.90/67.5 = 0.7985$ ).
- l 7/8/91 Waterspout flow divided by a ratio of 0.736 ( $36.5/0.736 = 49.59$ ); see Note "f" above for ratio derivation.
- m 7/8/91 Nelsons flow divided by a ratio of 0.7985 ( $86.5/0.7985 = 108.33$ ); see Note "k" for ratio derivation.
- n Measured at 60 gpm; based on comparison of flows in the other gulches between 10/14/92 and 10/28/92 measurement appears too low and is questionable; flow estimated to be higher at 67.5 gpm.
- o Measured at 74.07 gpm; measurement made twice and assumed reliable; because of low 10/14/92 measurement, flow estimated downward to 67.5.

Table 2  
 Average Summer Yield (June 14 through October 28) for  
 Combined Flow of Thicket Draw, Beans Gulch, Waterspout Gulch  
 and Nelsons Gulch, 44-Year Period 1948-92

Water Year	Annual Precip (In)	Gulch Yield (GPM)	Water Year	Annual Precip (In)	Gulch Yield (GPM)
1948 - 49	35.17	191	1970 - 71	46.24	241
1949 - 50	30.49	169	1971 - 72	31.57	174
1950 - 51	41.41	219	1972 - 73	44.62	234
1951 - 52	47.27	246	1973 - 74	54.84	281
1952 - 53	48.36	251	1974 - 75	40.99	217
1953 - 54	42.32	224	1975 - 76	28.8	162
1954 - 55	31.95	176	1976 - 77	16.56	106
1955 - 56	47.41	247	1977 - 78	47.95	249
1956 - 57	33.45	183	1978 - 79	31.87	176
1957 - 58	58.02	295	1979 - 80	41.28	219
1958 - 59	29.44	165	1980 - 81	30.25	168
1959 - 60	30.72	170	1981 - 82	43.67	230
1960 - 61	39.19	209	1982 - 83	50.45	261
1961 - 62	34.03	186	1983 - 84	36.4	196
1962 - 63	38.43	206	1984 - 85	30.56	170
1963 - 64	32.78	180	1985 - 86	42.41	224
1964 - 65	41.70	221	1986 - 87	31.46	174
1965 - 66	35.10	190	1987 - 88	29.8	166
1966 - 67	46.47	243	1988 - 89	42.25	223
1967 - 68	34.48	188	1989 - 90	35.56	193
1968 - 69	50.62	262	1990 - 91	24.17	140
1969 - 70	41.25	219	1991 - 92	32.53	179

Note - Average summer discharge = (precip x 4.57822) + 29.78191.  
 - Water year ending September 30.  
 - Precipitation from Ft. Bragg Station.

Table 3  
Analysis of Inflow to Drydock Gulch During Drawdown Test

Parameter	Period of Calculation				Total Period
	Draw-down w/o Rain	Draw-down	Draw-down + Recovery	Pretest	
<i>Inflow</i>					
Rain, Inches	0	1-3/4	2	0	2
<i>Outflow</i>					
Pumped, Inches	-2.801	-4.441	-4.441	0.000	-4.441
Evaporation, Inches	-0.125	-0.201	-0.284	-0.005	-0.290
Outflow-Inflow, Inches	-2.926	-2.893	-2.726	-0.005	-2.731
Change-in-storage, Inches	-2.500	-1.901	-0.070	0.086	0.017
Imbalance, Inches	0.426	0.991	2.656	0.091	2.748
Time increment, Minutes	2000	3220	4550	85	4635
Subsurface in, GPM	17.803	25.716	48.766	89.836	49.519

Note - Volume based on surface area of 134,012 ft<sup>2</sup>  
 - Total volume pumped 371,004 gallons (115.23 gpm).

Table 4  
Estimate of Drydock Gulch Summer Baseflow

Water Year	Average Summer Gulch Discharge	Ratio Gulch Discharge To 1991-92	Average Summer Drydock Discharge
	(GPM)		(GPM)
1974-75	217.44	1.184	28.88
1975-76	161.63	0.880	21.46
1976-77	105.60	0.575	14.02
1978-79	249.31	1.357	33.11
1990-91	140.44	0.765	18.65
1991-92	183.66	1.000	24.39 <sup>a</sup>

- Note - Water year ending September 1.  
 - Average summer flow for period June 14 through October 28.  
 - Drydock discharge equal to ratio times 1991-92 calculated summer flow.  
<sup>a</sup> 17.80 gpm, observed 10/27/92, divided by 0.73, ratio of October 27 discharge to average summer flow.

Table 5  
Ft Bragg Precipitation 44-Year Period 1948 - 1992

WATER YR END	1948	1949	1950	1951	1952	1953	1954	
OCT	0.00	1.49	0.92	7.15	3.44	0.14	2.49	
NOV	0.00	2.74	2.46	5.09	6.60	4.20	6.77	
DEC	0.00	6.58	3.08	6.11	13.41	14.97	2.57	
JAN	0.00	1.82	9.48	9.96	10.00	12.94	11.64	
FEB	0.00	7.02	4.76	6.44	4.90	1.21	3.85	
MAR	0.00	13.61	6.79	3.20	4.23	5.14	5.81	
APR	0.00	0.32	1.86	1.49	1.99	4.82	4.36	
MAY	0.00	1.28	0.80	1.85	0.90	2.50	0.00	
JUN	0.00	0.11	0.21	0.02	1.69	1.48	2.21	
JUL	0.05	0.10	0.00	0.03	0.00	0.00	0.02	
AUG	0.02	0.03	0.04	0.03	0.01	0.94	2.45	
SEP	1.44	0.07	0.09	0.04	0.10	0.02	0.15	
	-----	-----	-----	-----	-----	-----	-----	
WATER YR SUM	1.51	35.17	30.49	41.41	47.27	48.36	42.32	inches
	1947	1948	1949	1950	1951	1952	1953	
	1948	1949	1950	1951	1952	1953	1954	
INDEX		91.88	79.65	108.18	123.49	126.33	110.56	
INDEX DEV		-8.12	-20.35	8.18	23.49	26.33	10.56	
CUM DEV	0	-8.12	-28.47	-20.9	3.19	29.53	40.08	
WATER YR END	1955	1956	1957	1958	1959	1960	1961	
OCT	1.56	1.49	3.67	7.36	0.22	0.87	2.09	
NOV	7.69	7.75	0.43	3.03	2.04	0.08	6.20	
DEC	9.28	13.40	1.70	5.24	2.54	2.53	6.37	
JAN	4.59	14.92	5.08	8.31	11.93	7.22	4.24	
FEB	2.19	7.05	5.24	19.53	7.27	7.89	7.03	
MAR	0.91	0.93	7.84	6.90	2.65	7.71	7.38	
APR	5.09	0.71	2.59	5.63	0.41	2.16	2.15	
MAY	0.00	0.70	4.57	0.50	0.35	2.02	2.66	
JUN	0.02	0.44	0.08	1.20	0.07	0.00	0.24	
JUL	0.01	0.00	0.20	0.06	0.03	0.09	0.05	
AUG	0.00	0.00	0.00	0.08	0.04	0.09	0.27	
SEP	0.61	0.02	2.05	0.18	1.89	0.06	0.51	
	-----	-----	-----	-----	-----	-----	-----	
WATER YR SUM	31.95	47.41	33.45	58.02	29.44	30.72	39.19	inches
	1954	1955	1956	1957	1958	1959	1960	
	1955	1956	1957	1958	1959	1960	1961	
INDEX	83.47	123.85	87.38	151.57	76.91	80.25	102.38	
INDEX DEV	-16.53	23.85	-12.62	51.57	-23.09	-19.75	2.38	
CUM DEV	23.55	47.40	34.79	86.36	63.27	43.52	45.90	

Table 5 (continued)  
 Ft Bragg Precipitation 44-Year Period 1948 - 1992

WATER YR END	1962	1963	1964	1965	1966	1967	1968	
OCT	1.79	6.43	5.30	2.57	0.73	0.12	3.60	
NOV	6.48	3.16	10.10	9.63	10.31	9.92	3.90	
DEC	4.61	4.35	2.18	14.58	3.94	7.22	6.51	
JAN	3.44	2.79	7.58	5.27	8.39	9.28	8.05	
FEB	7.18	3.86	0.79	1.87	4.83	1.03	4.33	
MAR	5.53	7.02	3.99	2.06	3.71	9.33	4.43	
APR	1.44	9.43	0.64	4.96	2.18	7.59	0.56	
MAY	0.39	0.98	1.29	0.13	0.22	1.12	1.19	
JUN	0.03	0.14	0.60	0.14	0.10	0.33	0.09	
JUL	0.09	0.01	0.18	0.11	0.03	0.06	0.05	
AUG	1.98	0.07	0.07	0.24	0.22	0.02	1.34	
SEP	1.07	0.19	0.06	0.14	0.44	0.45	0.43	
	-----	-----	-----	-----	-----	-----	-----	
WATER YR SUM	34.03	38.43	32.78	41.70	35.10	46.47	34.48	inches
	1961	1962	1963	1964	1965	1966	1967	
	1962	1963	1964	1965	1966	1967	1968	
INDEX	88.90	100.39	85.63	108.94	91.69	121.40	90.07	
INDEX DEV	-11.10	0.39	-14.37	8.94	-8.31	21.40	-9.93	
CUM DEV	34.80	35.19	20.82	29.76	21.45	42.85	32.93	
WATER YR END	1969	1970	1971	1972	1973	1974	1975	
OCT	1.84	2.77	3.32	1.16	3.18	5.67	2.41	
NOV	4.88	2.76	8.76	3.89	8.02	12.98	1.92	
DEC	12.81	14.30	10.81	5.79	6.28	7.39	6.62	
JAN	13.50	13.43	8.56	4.78	10.80	7.60	4.32	
FEB	10.67	3.28	1.54	5.79	7.87	5.18	10.22	
MAR	2.33	3.25	8.35	3.83	5.30	9.84	11.38	
APR	3.23	0.59	2.33	2.17	0.92	4.37	2.47	
MAY	0.29	0.40	0.83	0.71	0.49	0.31	0.34	
JUN	0.44	0.37	0.48	0.50	0.06	0.34	0.17	
JUL	0.02	0.00	0.03	0.04	0.08	0.85	0.53	
AUG	0.03	0.03	0.76	0.22	0.16	0.18	0.49	
SEP	0.58	0.07	0.47	2.69	1.46	0.13	0.12	
	-----	-----	-----	-----	-----	-----	-----	
WATER YR SUM	50.62	41.25	46.24	31.57	44.62	54.84	40.99	inches
	1968	1969	1970	1971	1972	1973	1974	
	1969	1970	1971	1972	1973	1974	1975	
INDEX	132.24	107.76	120.80	82.47	116.56	143.26	107.08	
INDEX DEV	32.24	7.76	20.80	-17.53	16.56	43.26	7.08	
CUM DEV	65.16	72.92	93.72	76.19	92.76	136.02	143.10	



Table 5 (continued)  
Ft Bragg Precipitation 44-Year Period 1948 - 1992

WATER YR END	1976	1977	1978	1979	1980	1981	1982	
OCT	4.72	0.19	2.38	0.04	6.00	2.41	4.55	
NOV	2.59	2.61	3.83	1.26	9.72	1.49	8.25	
DEC	3.96	0.68	8.37	2.11	4.78	4.47	8.10	
JAN	1.31	1.94	11.24	7.73	3.23	8.89	5.70	
FEB	7.56	2.43	6.59	10.84	9.42	4.73	4.31	
MAR	2.30	2.45	5.60	4.91	3.31	3.98	7.16	
APR	4.08	0.57	6.23	2.37	3.90	0.58	4.75	
MAY	0.19	1.93	0.69	1.91	0.50	1.87	0.01	
JUN	0.05	0.06	0.07	0.03	0.26	0.14	0.43	
JUL	0.36	0.03	0.07	0.35	0.03	0.00	0.06	
AUG	1.58	0.58	0.40	0.01	0.01	0.06	0.06	
SEP	0.10	3.09	2.48	0.31	0.12	1.63	0.29	
	-----	-----	-----	-----	-----	-----	-----	
WATER YR SUM	28.80	16.56	47.95	31.87	41.28	30.25	43.67	inches
	1975	1976	1977	1978	1979	1980	1981	
	1976	1977	1978	1979	1980	1981	1982	
INDEX	75.24	43.26	125.26	83.26	107.84	79.02	114.08	
INDEX DEV	-24.76	-56.74	25.26	-16.74	7.84	-20.98	14.08	
CUM DEV	118.34	61.60	86.86	70.12	77.96	56.98	71.06	
WATER YR END	1983	1984	1985	1986	1987	1988	1989	
OCT	4.73	0.86	3.54	2.58	1.70	0.88	1.22	
NOV	9.34	11.44	13.64	4.78	1.39	5.24	11.46	
DEC	7.42	13.53	0.00	4.09	5.34	11.30	5.41	
JAN	7.36	0.55	1.26	6.81	7.54	4.98	3.08	
FEB	11.67	3.63	3.82	11.83	5.28	0.12	1.89	
MAR	0.00	3.67	6.46	7.91	8.25	1.06	12.53	
APR	4.84	0.00	0.24	0.98	0.68	2.11	2.49	
MAY	1.10	1.32	0.39	0.68	0.77	1.24	0.96	
JUN	0.16	0.76	0.06	0.28	0.17	2.79	0.57	
JUL	0.46	0.04	0.10	0.00	0.28	0.03	0.00	
AUG	3.00	0.09	0.14	0.07	0.06	0.00	0.24	
SEP	0.37	0.51	0.91	2.40	0.00	0.05	2.40	
	-----	-----	-----	-----	-----	-----	-----	
WATER YR SUM	50.45	36.40	30.56	42.41	31.46	29.80	42.25	inches
	1982	1983	1984	1985	1986	1987	1988	
	1983	1984	1985	1986	1987	1988	1989	
INDEX	131.79	95.09	79.83	110.79	82.19	77.85	110.37	
INDEX DEV	31.79	-4.91	-20.17	10.79	-17.81	-22.15	10.37	
CUM DEV	102.86	97.95	77.78	88.58	70.76	48.61	58.98	

Table 5 (continued)  
 Ft Bragg Precipitation 44-Year Period 1948 - 1992

WATER YR END	1990	1991	1992	
OCT	6.96	1.92	1.95	
NOV	1.97	0.98	2.21	
DEC	0.32	2.15	4.71	
JAN	7.85	1.49	4.01	
FEB	3.72	3.65	9.88	
MAR	3.31	10.06	5.39	
APR	1.32	1.57	2.43	
MAY	9.46	1.43	0.00	
JUN	0.21	0.50	1.82	
JUL	0.06	0.12	0.13	
AUG	0.16	0.28		
SEP	0.22	0.02		
	-----	-----	-----	
WATER YR SUM	35.56	24.17	32.53	inches
	1989	1990	1991	
	1990	1991	1992	
INDEX	92.90	63.14	84.98	
INDEX DEV	-7.10	-36.86	-15.02	
CUM DEV	51.88	15.02	0.00	

AVERAGE ANNUAL PRECIPITATION 38.28 INCHES

Table 6  
Annual Minimum Summer Discharge of Lower Gulches and  
Drydock Reservoir As A Function of Reservoir Capacity

Water Year	Annual Precip  (Inches)	Average Summer Discharge			
		Maximum reservoir capacity, AF:			
		7.2	15	25	40
		(GPM)			
1948 - 49	35.17	217	229	244	266
1949 - 50	30.49	193	205	220	242
1950 - 51	41.41	249	261	276	298
1951 - 52	47.27	279	291	306	328
1952 - 53	48.36	284	296	311	334
1953 - 54	42.32	254	265	280	303
1954 - 55	31.95	200	212	227	250
1955 - 56	47.41	280	291	306	329
1956 - 57	33.45	208	220	235	258
1957 - 58	58.02	334	346	361	383
1958 - 59	29.44	188	199	214	237
1959 - 60	30.72	194	206	221	244
1960 - 61	39.19	238	249	264	287
1961 - 62	34.03	211	223	238	261
1962 - 63	38.43	234	245	260	283
1963 - 64	32.78	205	216	232	254
1964 - 65	41.70	250	262	277	300
1965 - 66	35.10	217	228	243	266
1966 - 67	46.47	275	287	302	324
1967 - 68	34.48	213	225	240	263
1968 - 69	50.62	296	308	323	345
1969 - 70	41.25	248	260	275	298
1970 - 71	46.24	274	285	300	323
1971 - 72	31.57	199	210	225	248
1972 - 73	44.62	265	277	292	315
1973 - 74	54.84	318	329	344	367
1974 - 75	40.99	247	259	274	296
1975 - 76	28.80	184	196	211	234
1976 - 77	16.56	122	133	149	171
1977 - 78	47.95	282	294	309	332
1978 - 79	31.87	200	212	227	250
1979 - 80	41.28	248	260	275	298
1980 - 81	30.25	192	204	219	241
1981 - 82	43.67	260	272	287	310
1982 - 83	50.45	295	307	322	345
1983 - 84	36.40	223	235	250	273

Table 6 (continued)  
Annual Minimum Summer Discharge of Lower Gulches and  
Drydock Reservoir As A Function of Reservoir Capacity

Water Year	Annual Precip	Average Summer Discharge			
		Maximum reservoir capacity, AF:			
		7.2	15	25	40
	(Inches)	(GPM)			
1984 - 85	30.56	193	205	220	243
1985 - 86	42.41	254	266	281	303
1986 - 87	31.46	198	210	225	247
1987 - 88	29.80	189	201	216	239
1988 - 89	42.25	253	265	280	303
1989 - 90	35.56	219	231	246	268
1990 - 91	24.17	161	172	188	210
1991 - 92	32.53	203	215	230	253

- Note - Summer-flow period June 1 through November 1
- 7.2-AF reservoir (4.0 ft deep) = (precip x 5.117408) + 36.97192
  - 15-AF reservoir (6.3 ft deep) = (precip x 5.117408) + 48.73796
  - 25-AF reservoir (9.2 ft deep) = (precip x 5.117408) + 63.82263
  - 40-AF reservoir (13.6 ft deep) = (precip x 5.117408) + 86.44963

# 1991 OBSERVED AND ESTIMATED DISCHARGE FROM GULCHES

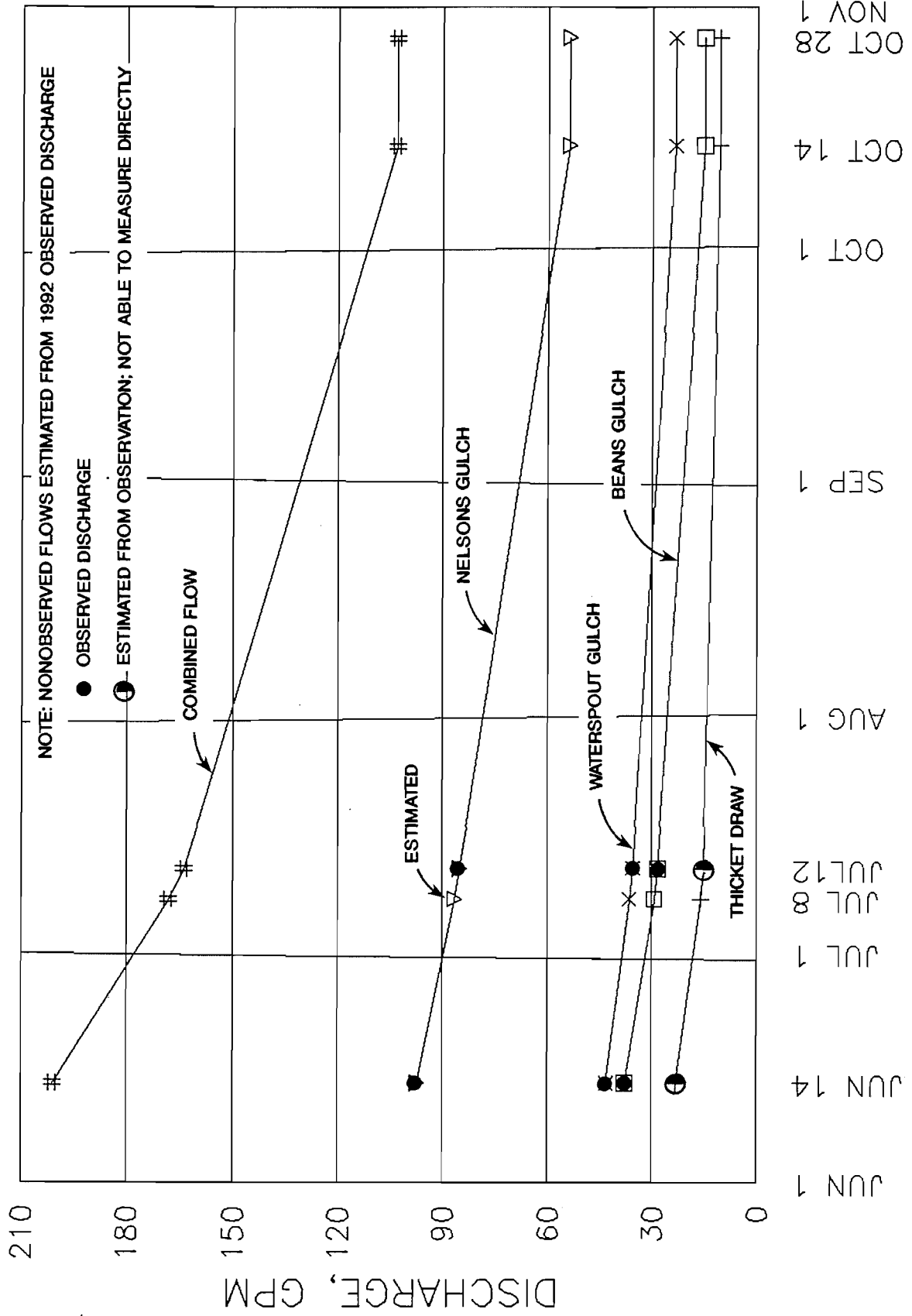


FIGURE 1

# 1992 OBSERVED AND ESTIMATED DISCHARGE FROM GULCHES

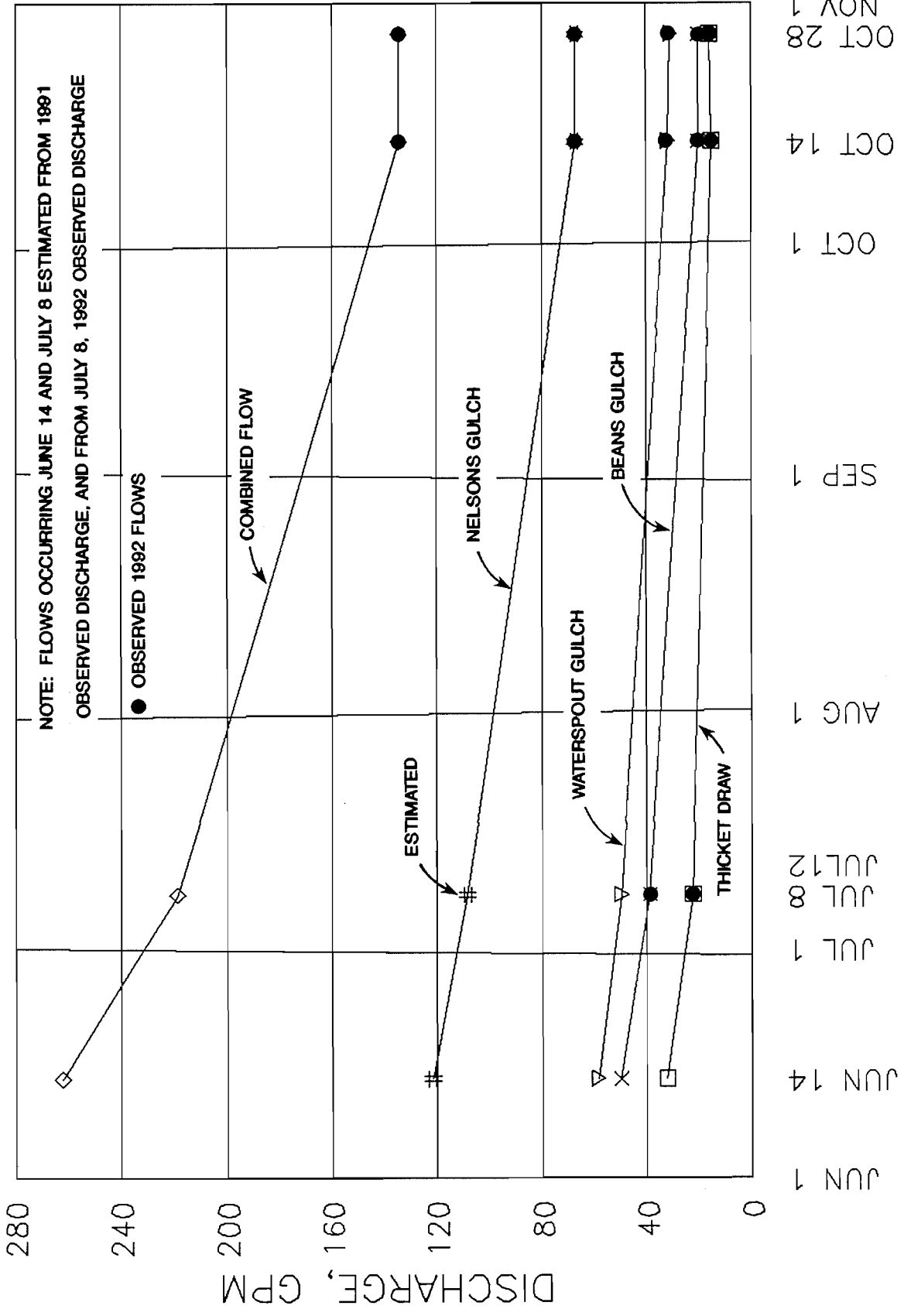


FIGURE 2

# GULCHES MONTHLY DISTRIBUTION OF FLOW

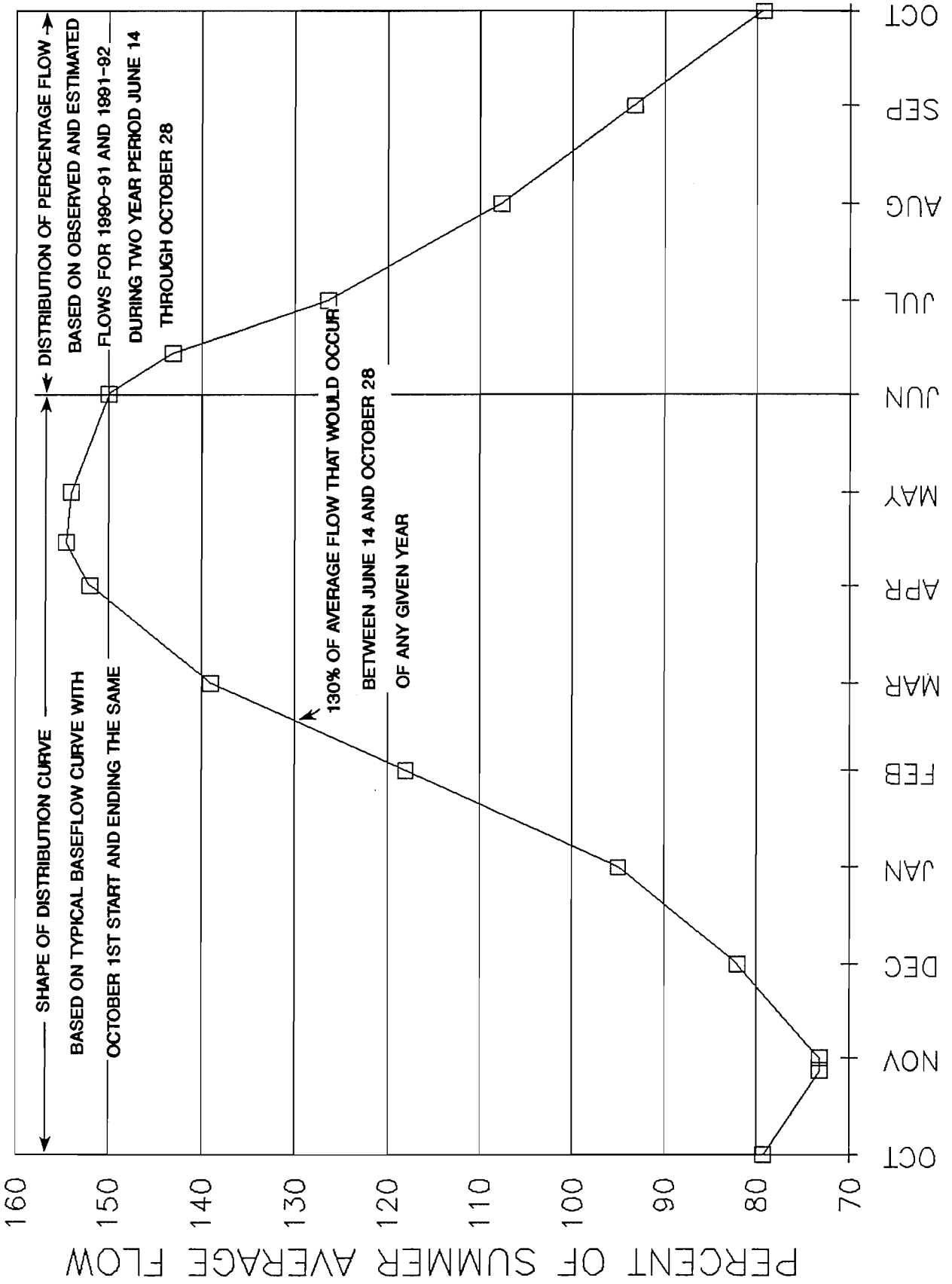


FIGURE 3

# TOTAL UNIT FLOW

NAVARRO RIVER - WATER YEAR 1975

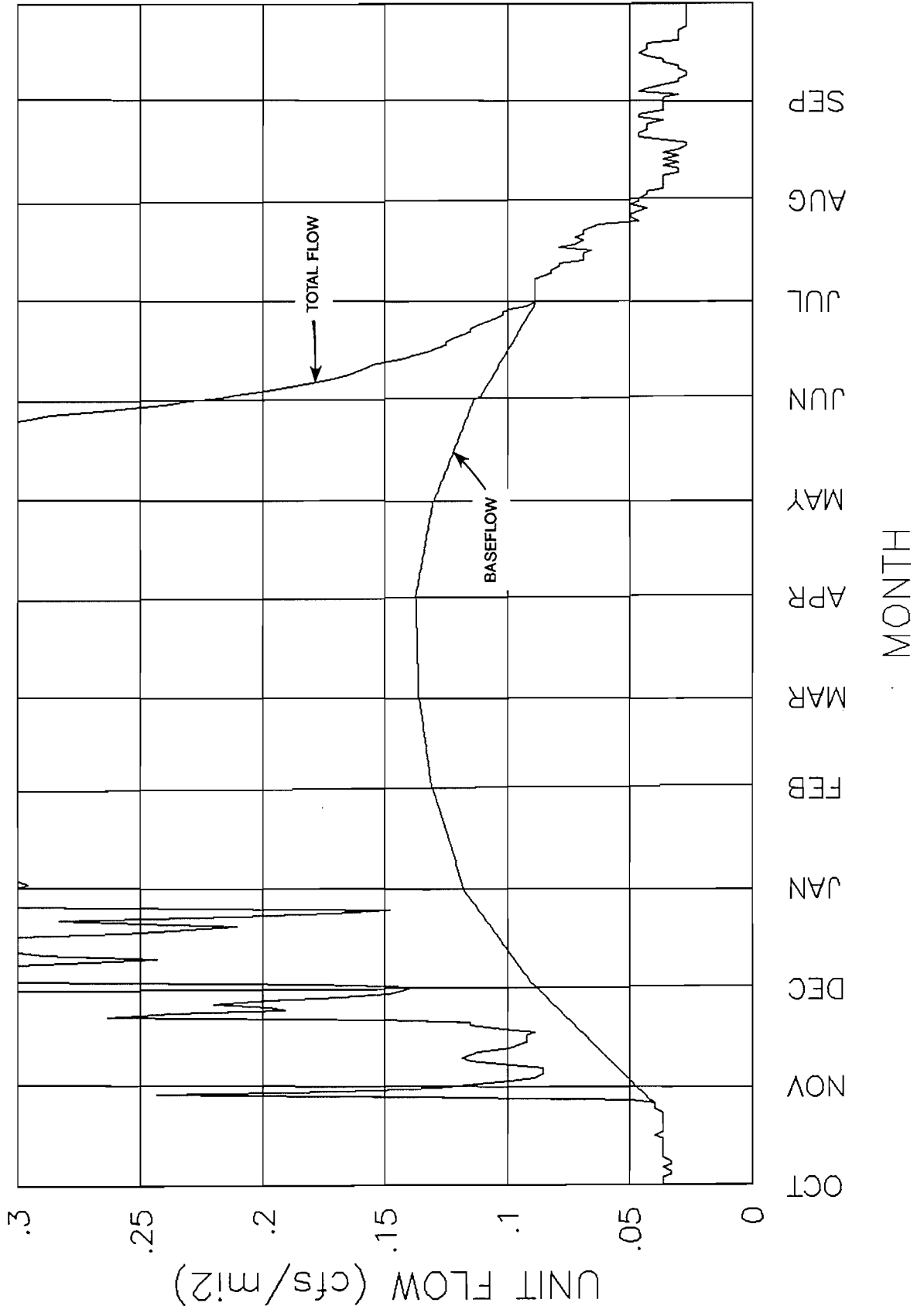
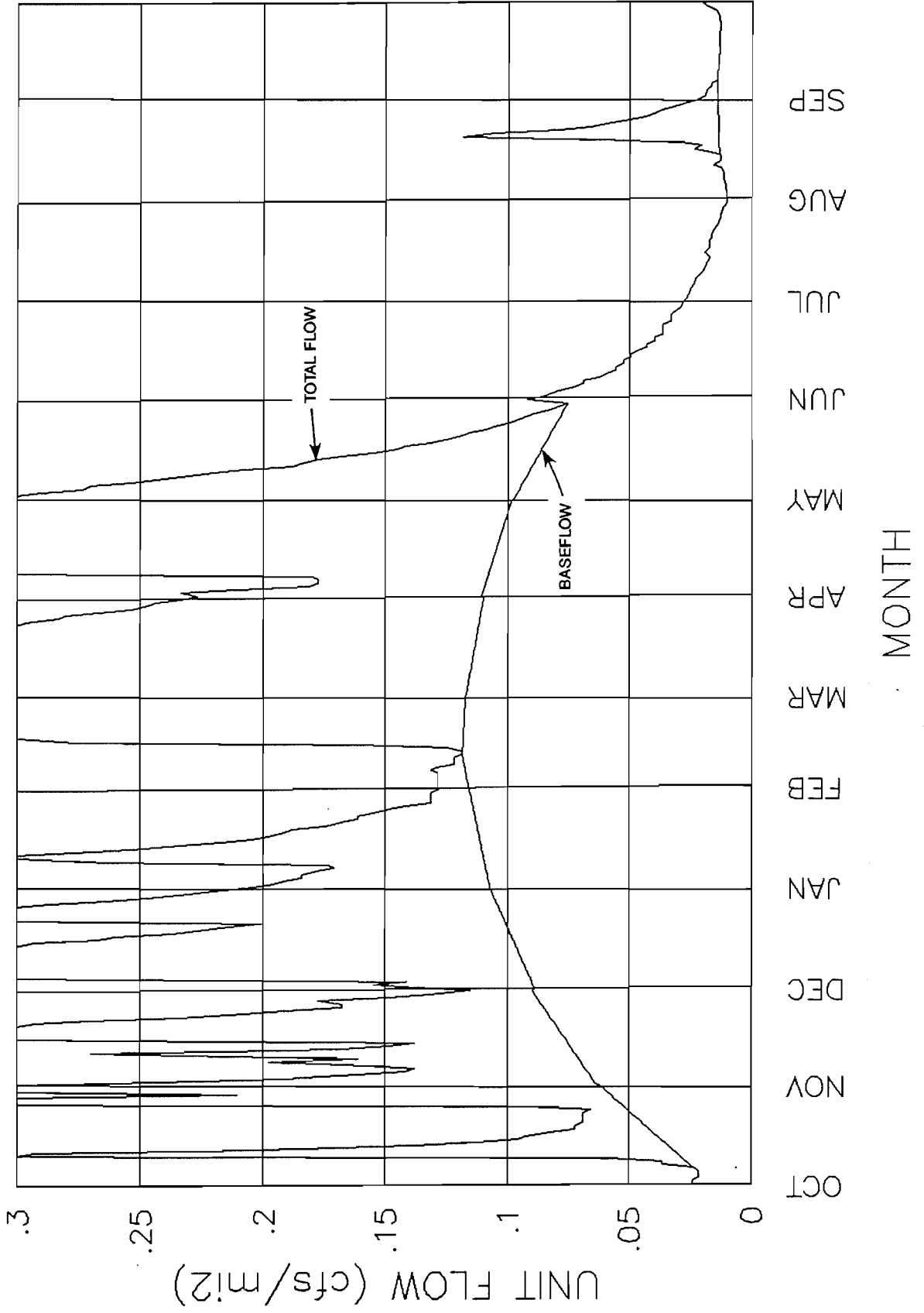


FIGURE 4



# TOTAL UNIT FLOW

NAVARRO RIVER - WATER YEAR 1976



# TOTAL UNIT FLOW NAVARRO RIVER - WATER YEAR 1977

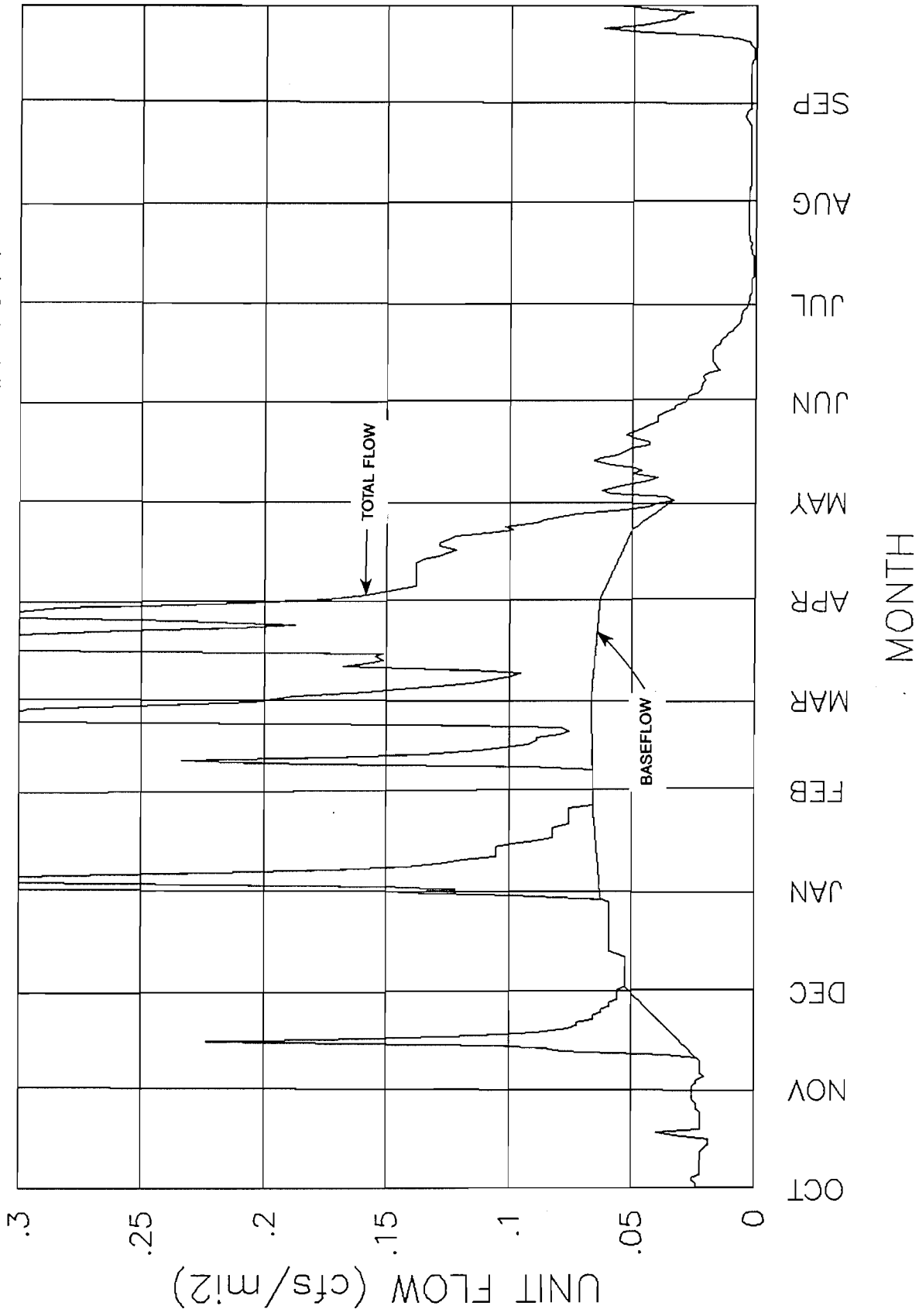
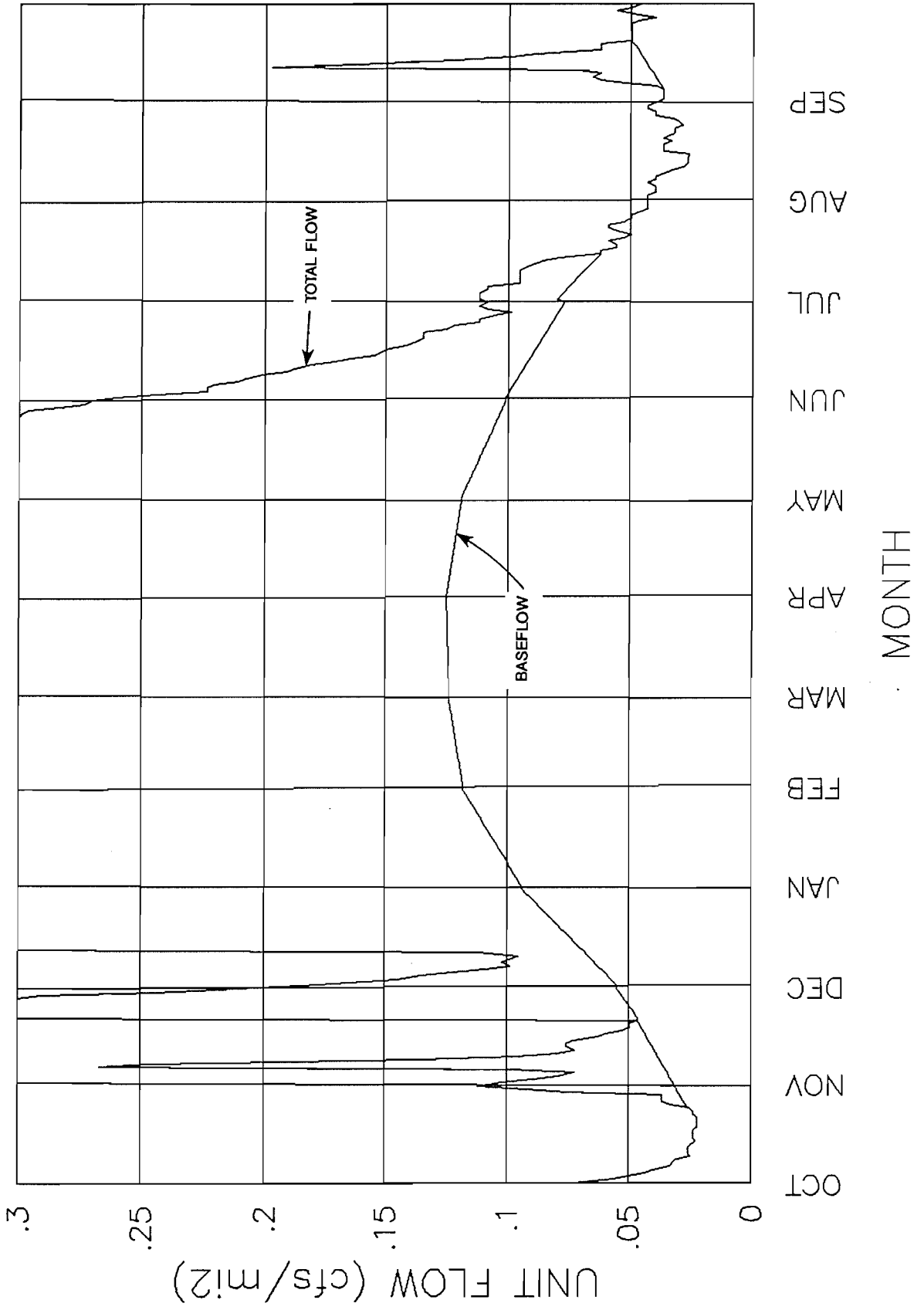


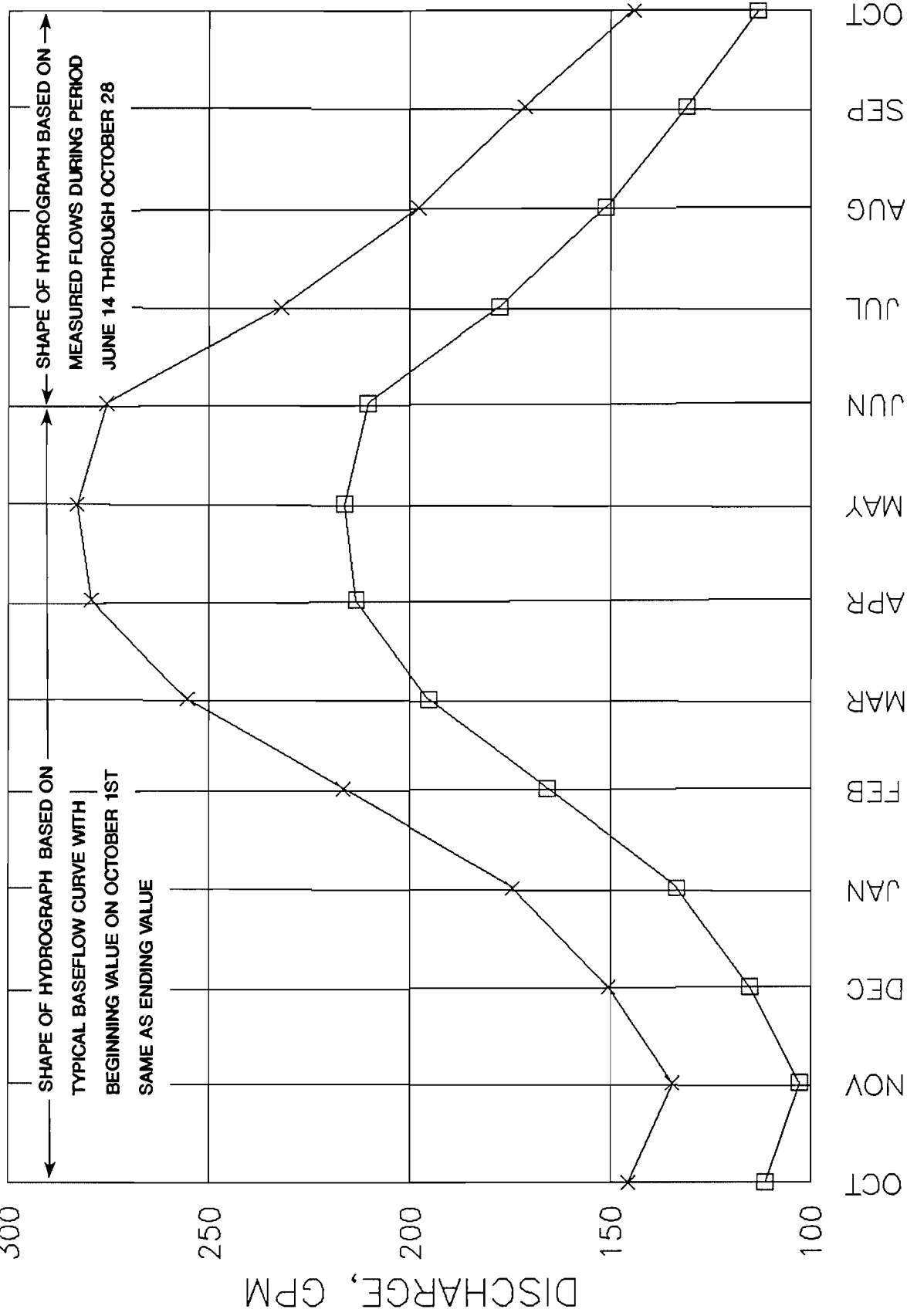
FIGURE 6

# TOTAL UNIT FLOW

NAVARRO RIVER - WATER YEAR 1978



# GULCHES COMBINED DISCHARGE, 1990-91 AND 1991-92



MONTHLY PERIODS BEGINNING OCTOBER 1

# COMBINED GULCHES SUMMER DISCHARGE VS RAINFALL

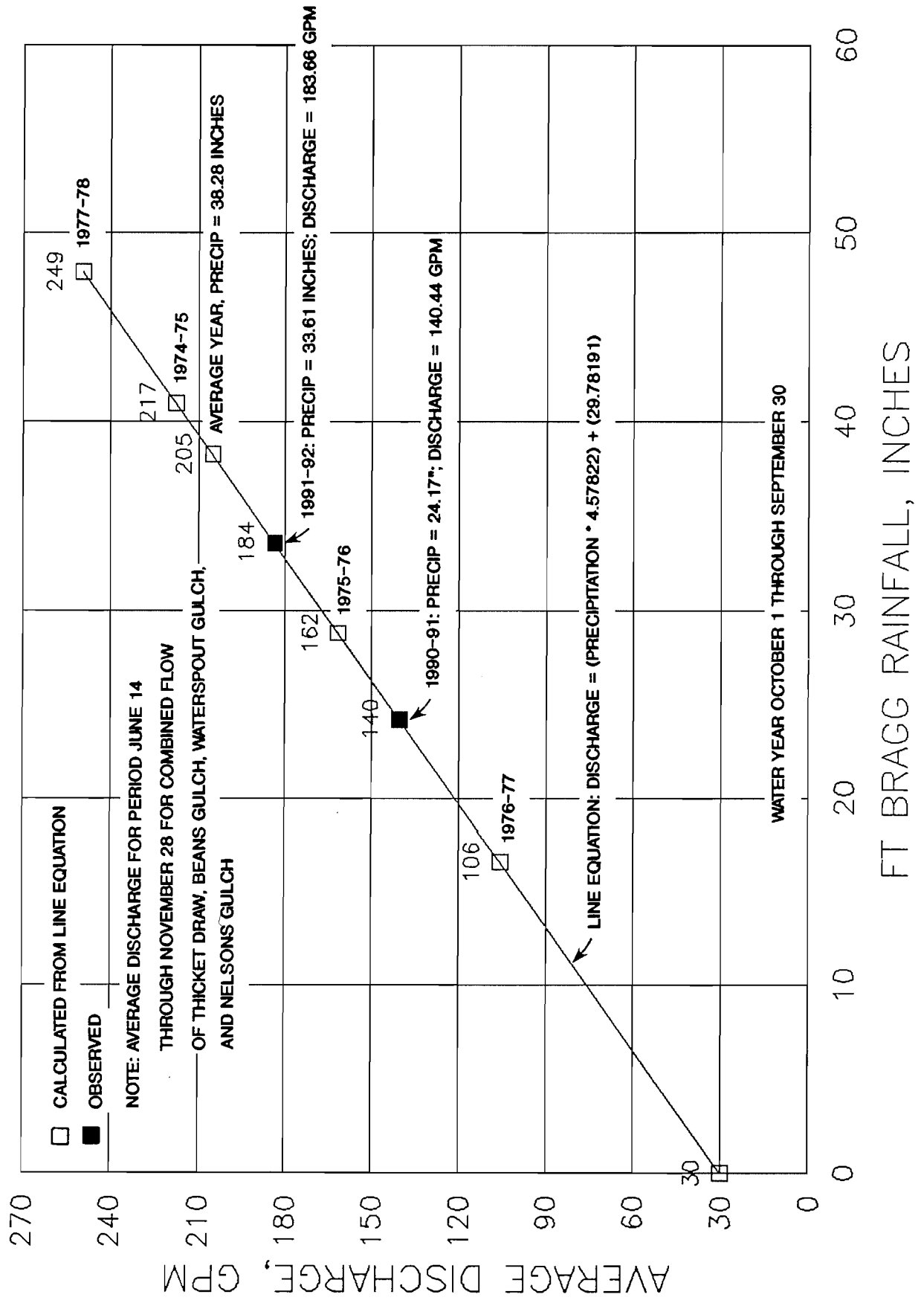
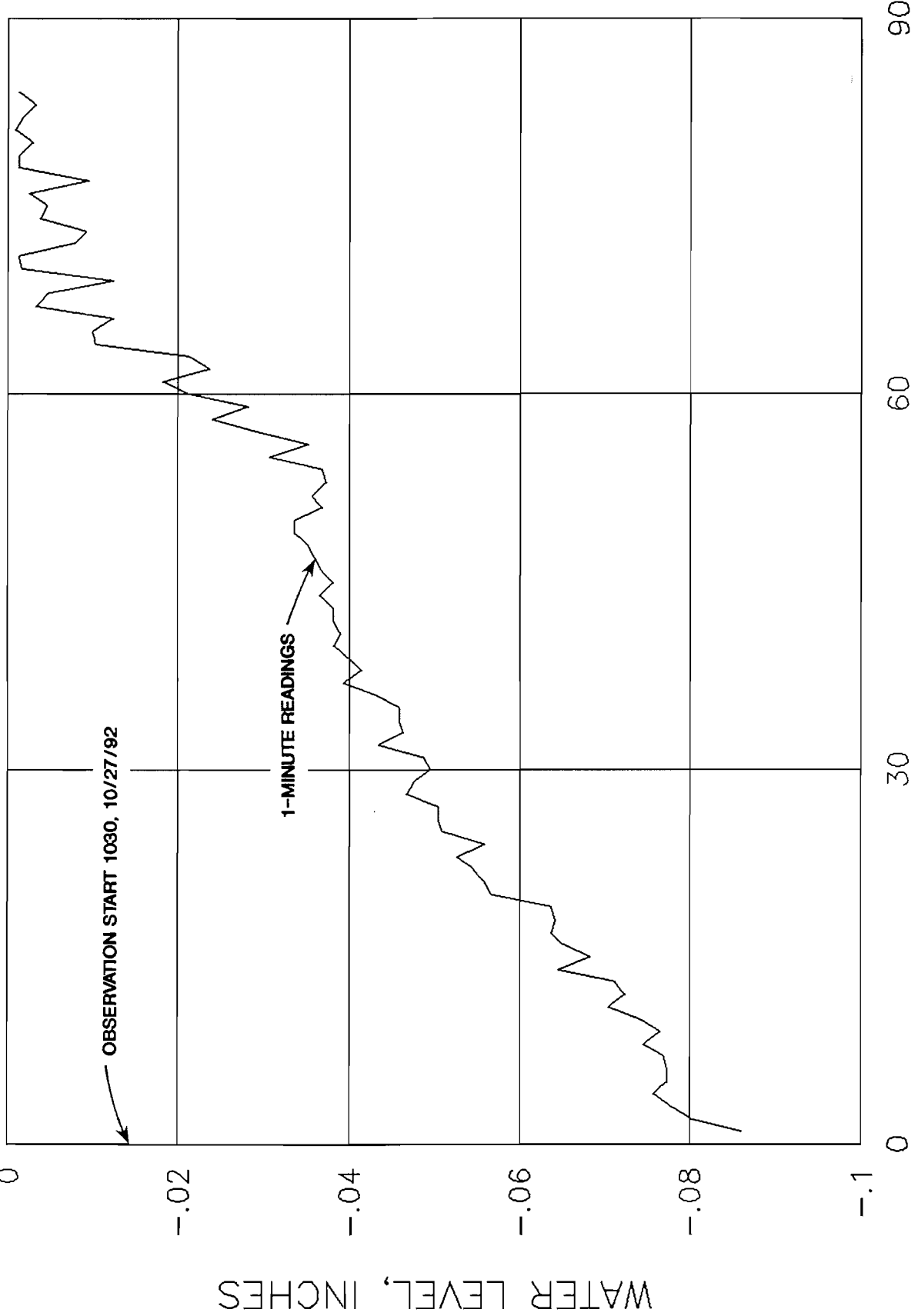


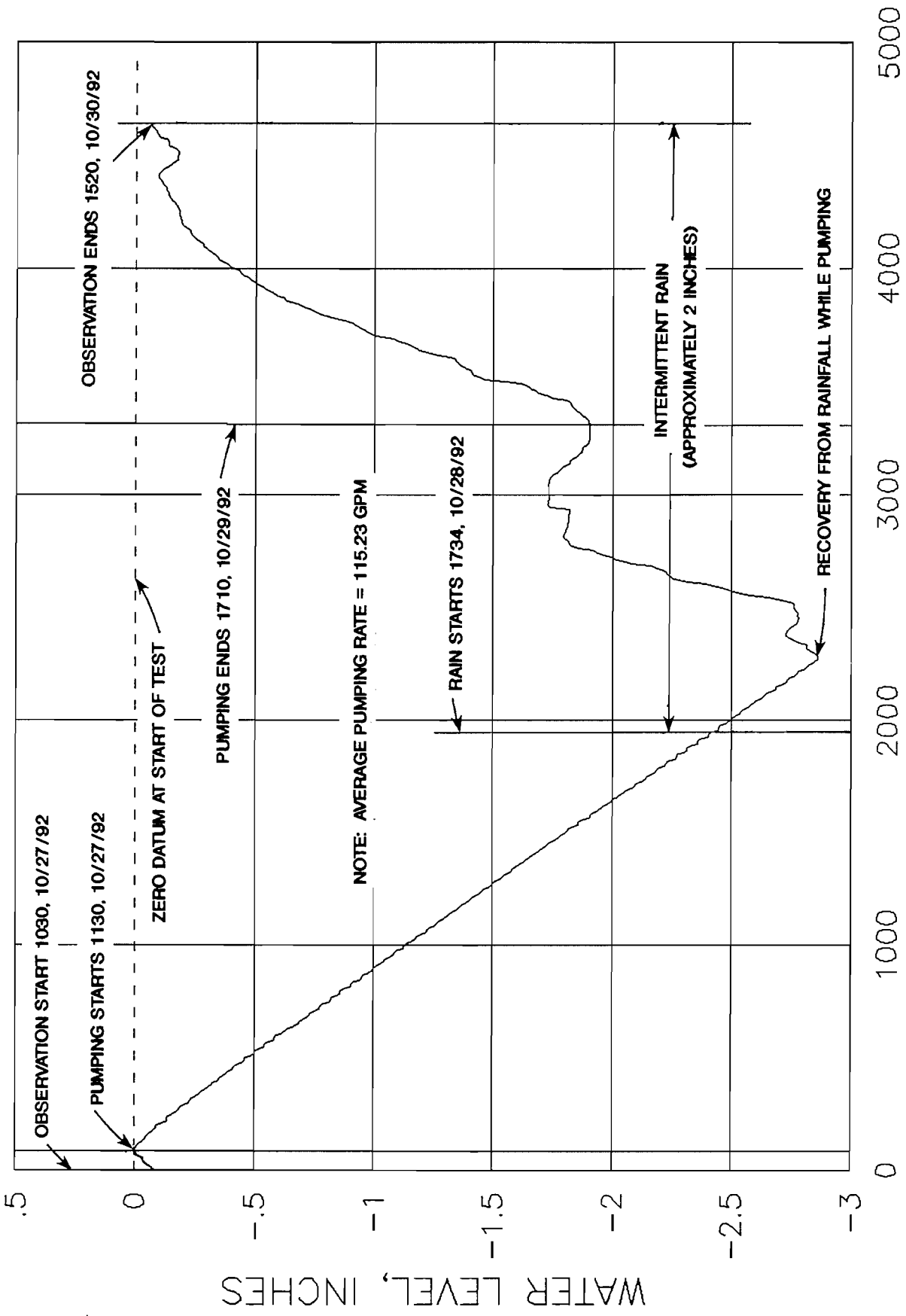
FIGURE 9

# WATER LEVEL DRYDOCK GULCH PRIOR TO START OF PUMPING TEST



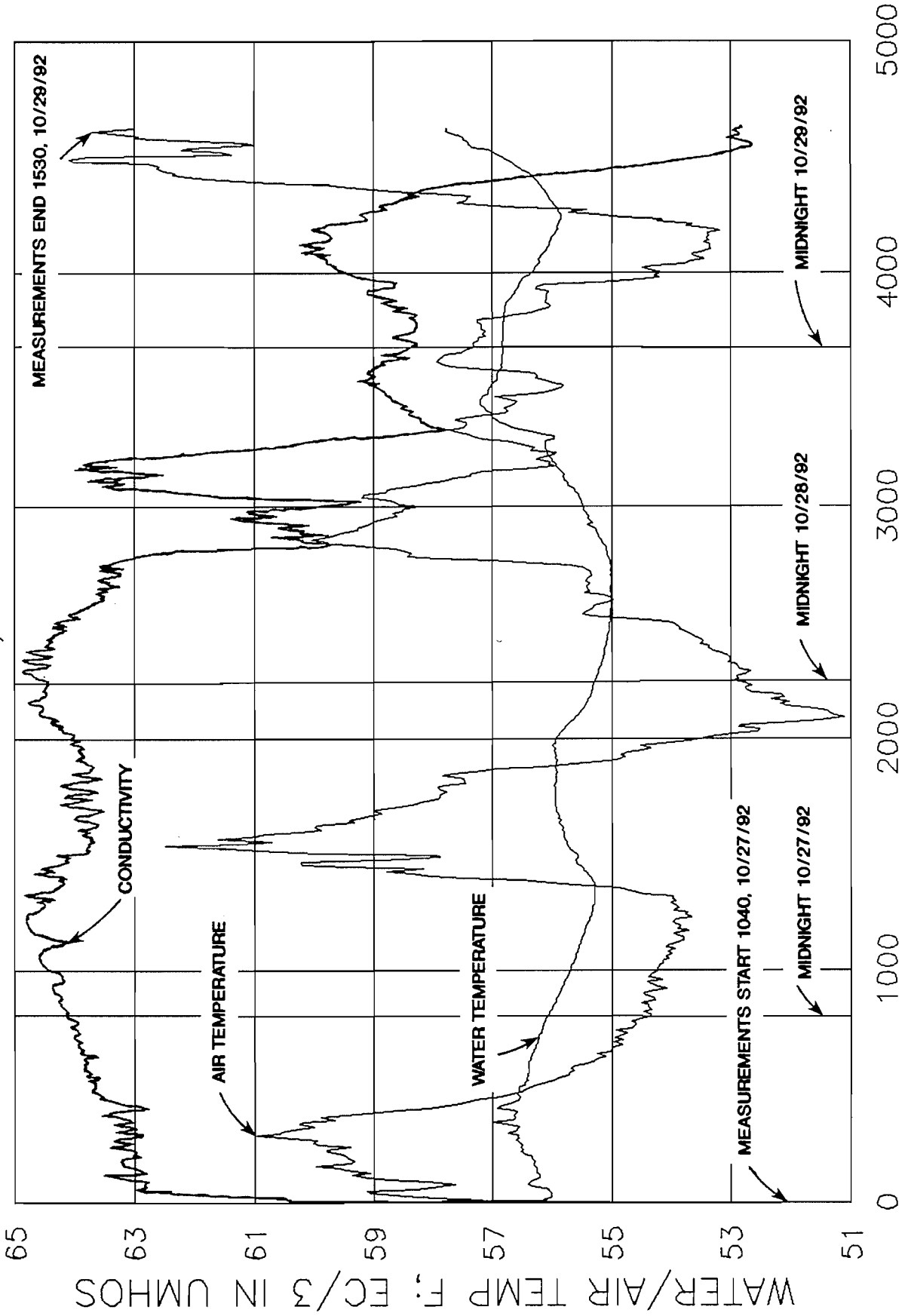
TIME SINCE OBSERVATION BEGAN, MINUTES

# DRAWDOWN AND RECOVERY OF DRYDOCK GULCH



TIME SINCE OBSERVATION BEGAN, MINUTES

# DRYDOCK GULCH AIR/WATER TEMP AND EC



TIME SINCE MEASUREMENTS BEGAN, MINUTES



# EVAPORATION VS. TEMPERATURE

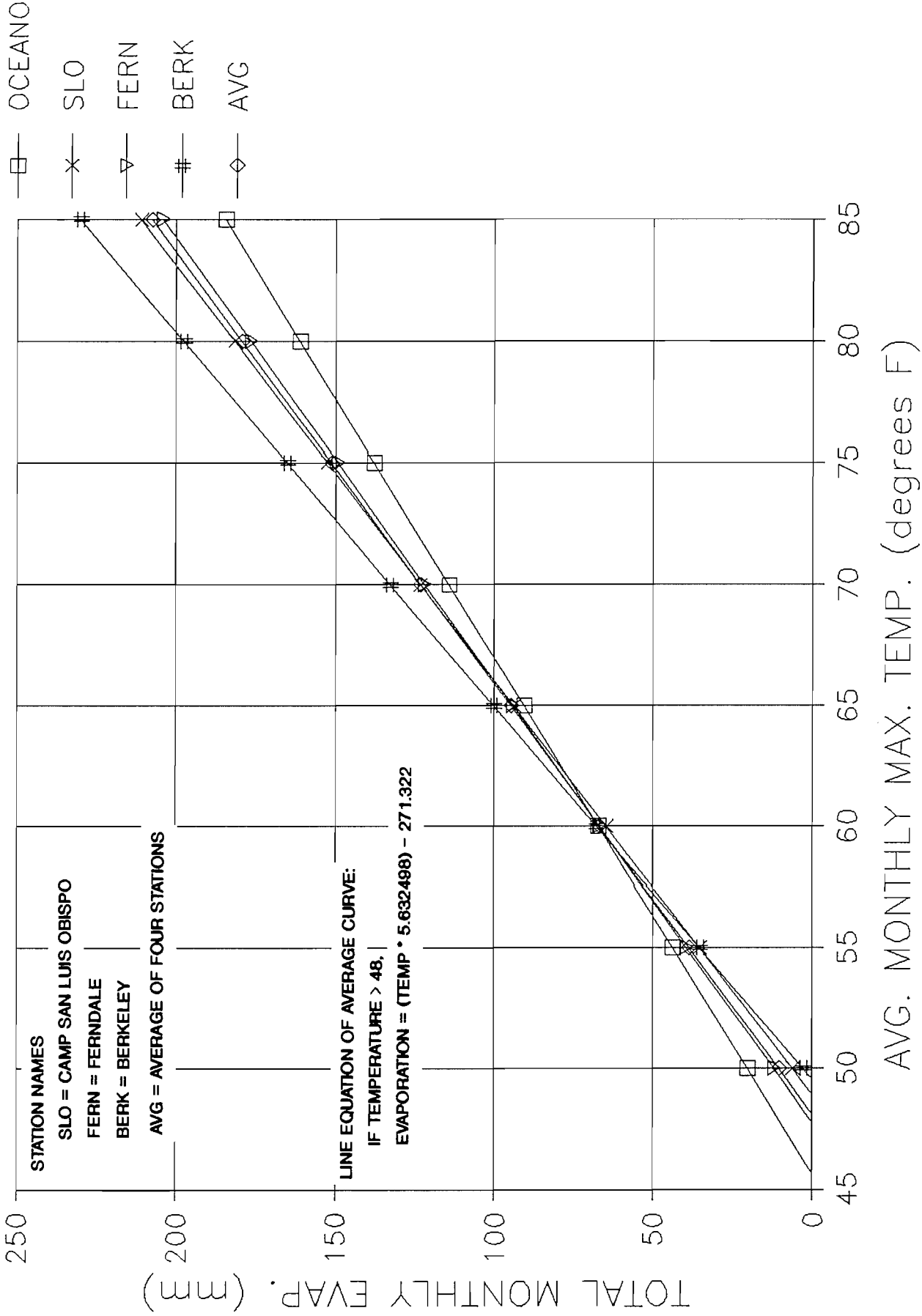
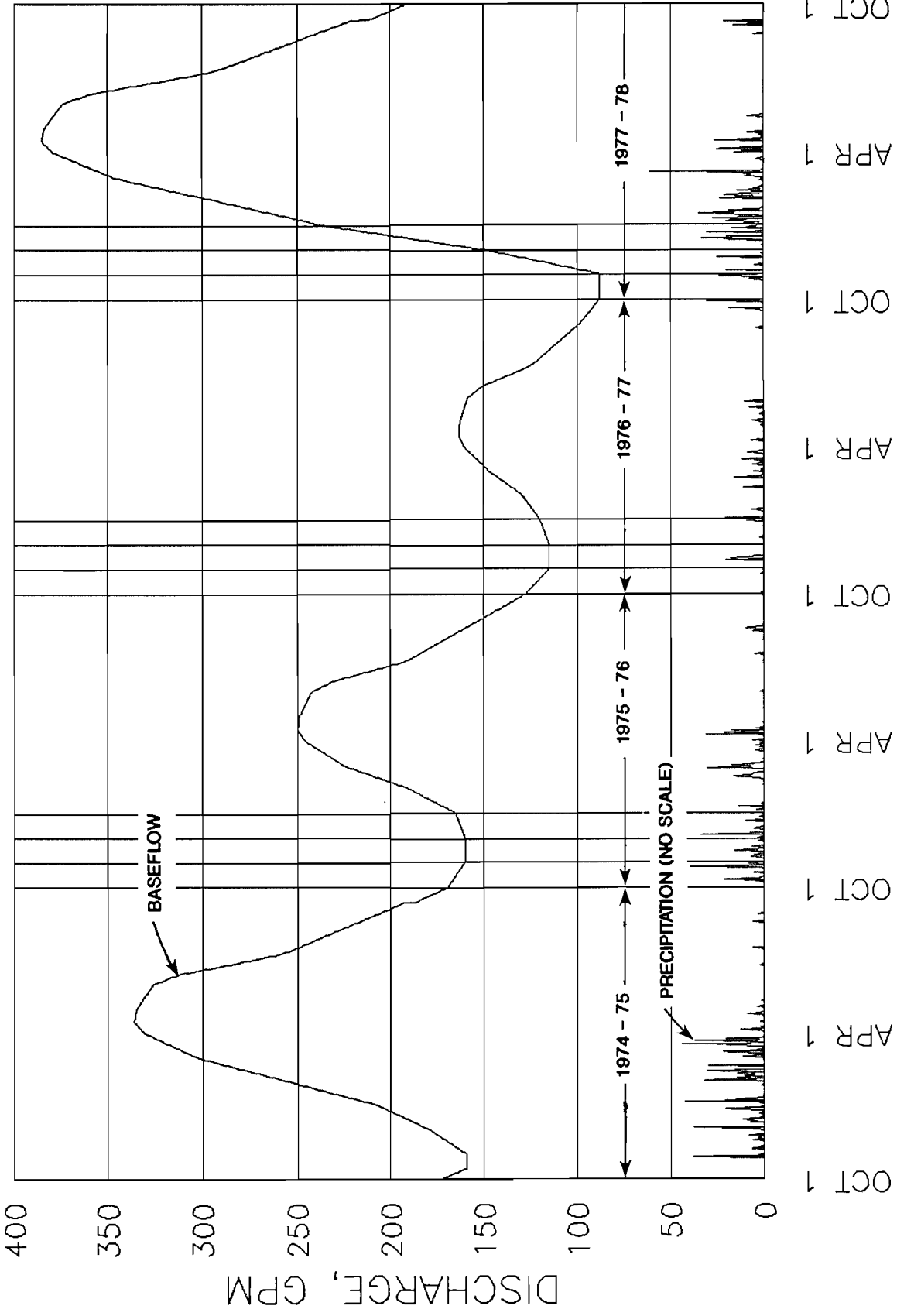


FIGURE 13

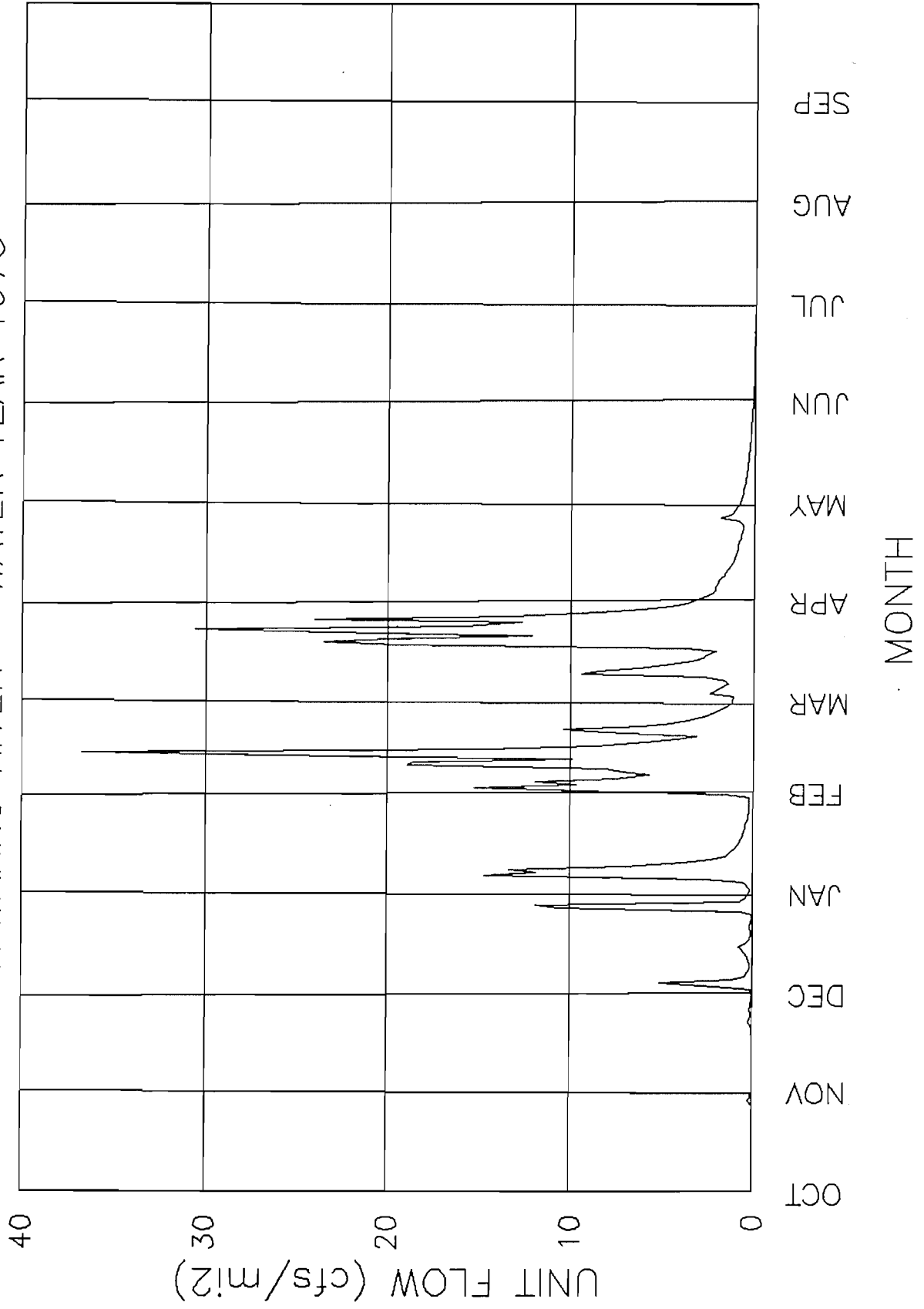
# GULCHES BASEFLOW AND PRECIPITATION, 1974-78



DAILY TIME STEPS

# STORM-WATER RUNOFF UNIT FLOW

NAVARRO RIVER - WATER YEAR 1975



# STORM—WATER RUNOFF UNIT FLOW NAVARRO RIVER — WATER YEAR 1976

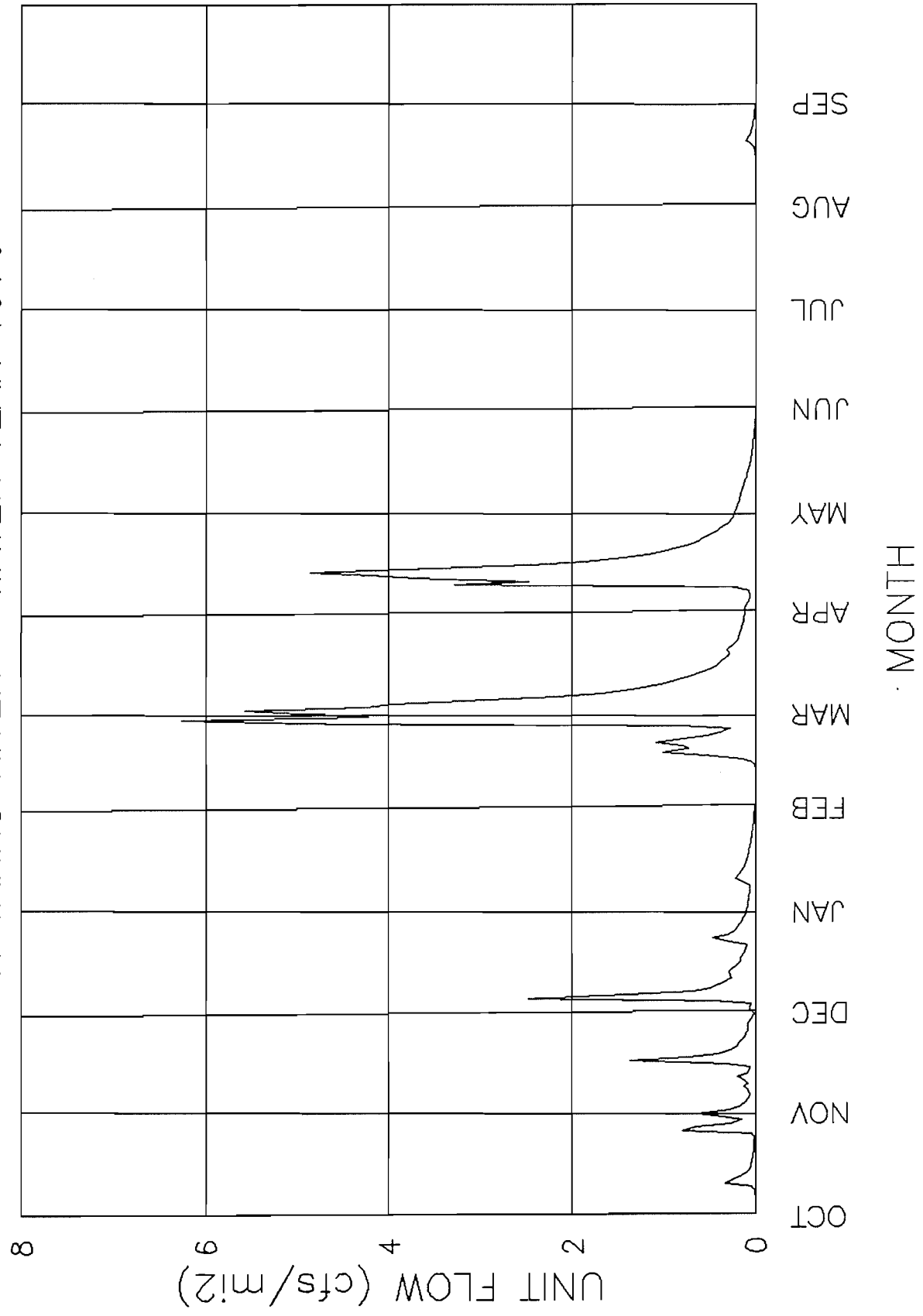


FIGURE 16

# STORM—WATER RUNOFF UNIT FLOW

NAVARRO RIVER — WATER YEAR 1977

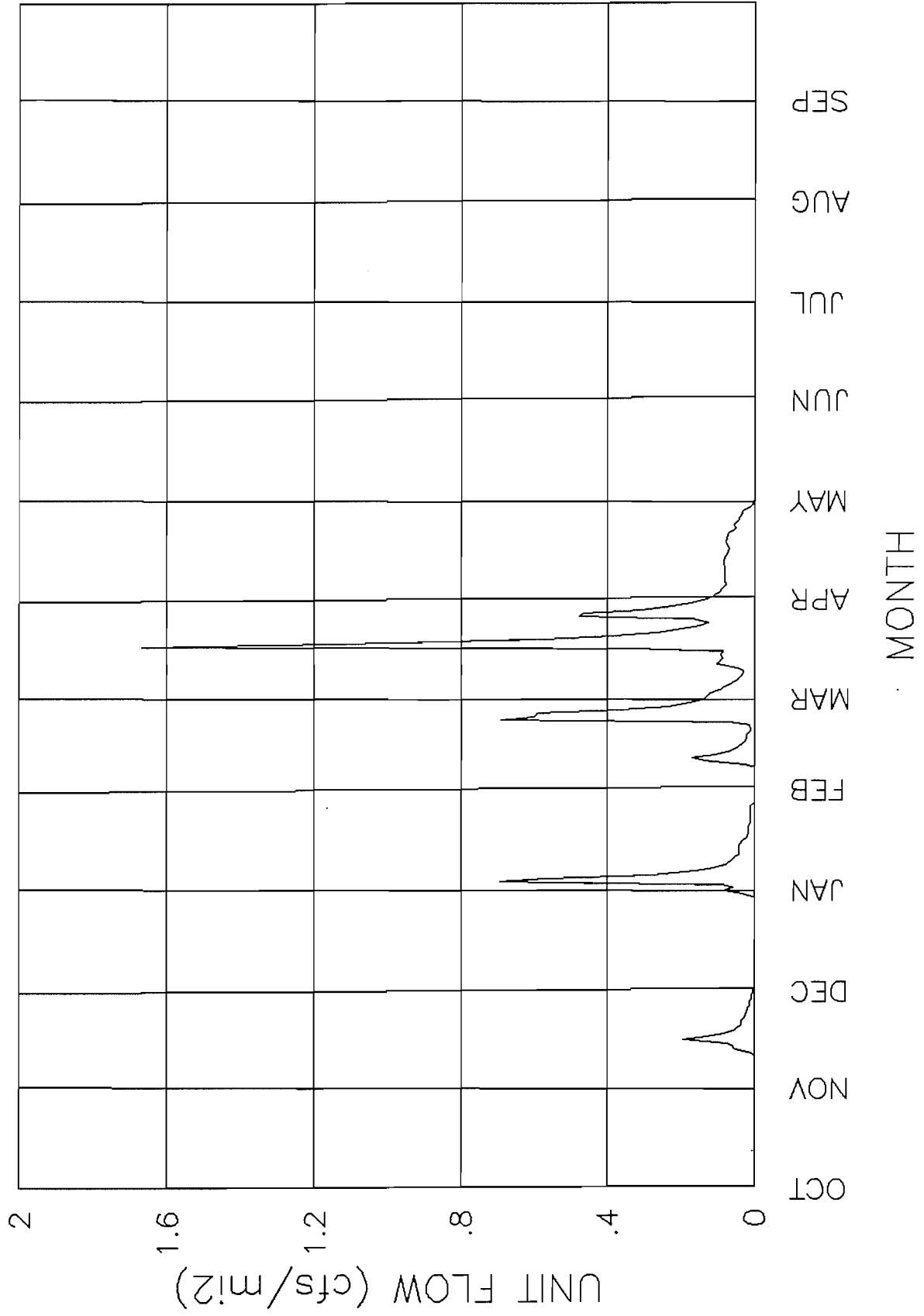


FIGURE 17

# STORM-WATER RUNOFF UNIT FLOW

NAVARRO RIVER - WATER YEAR 1978

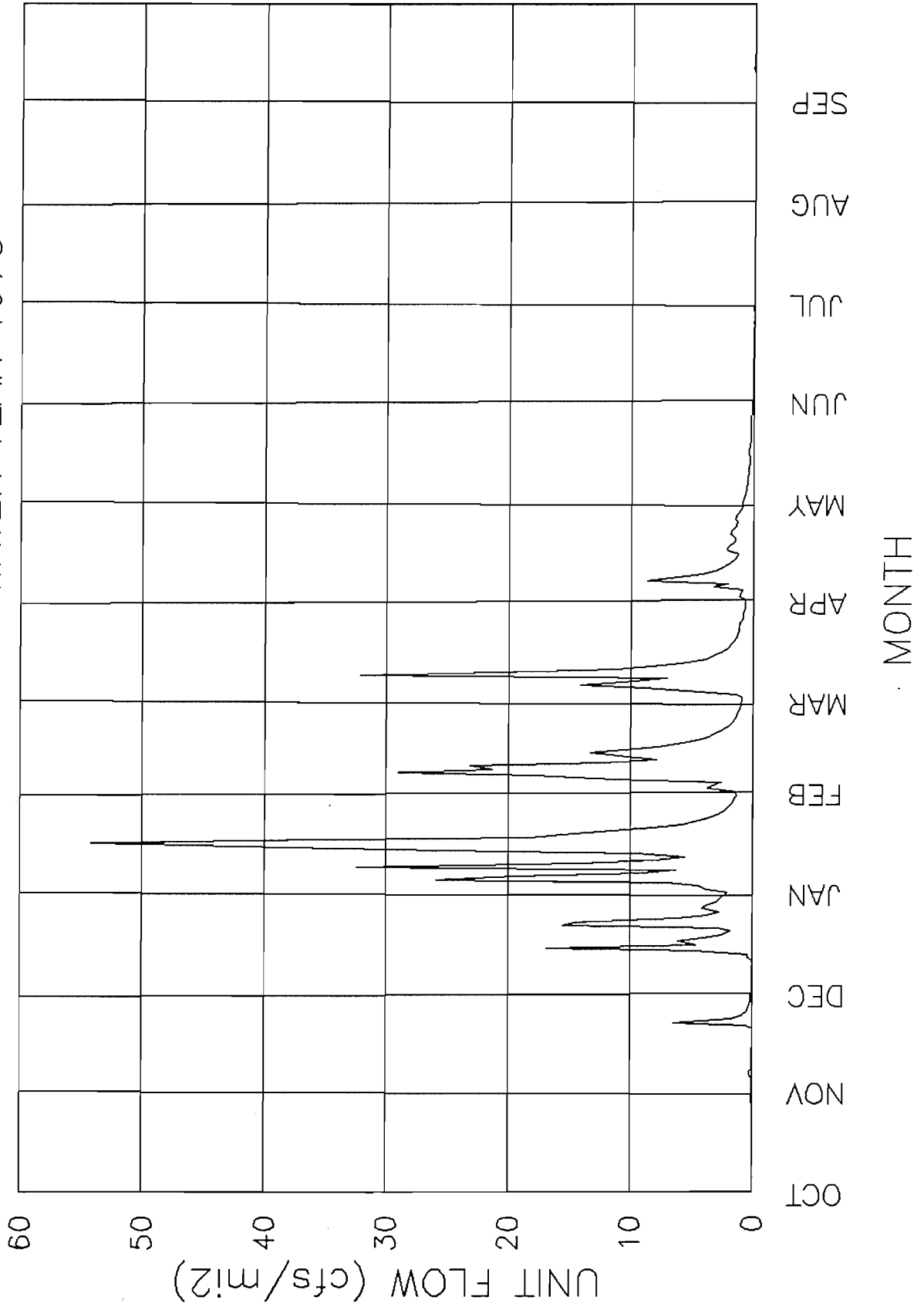


FIGURE 18

# EVAPORATION VS. TEMPERATURE

BERKELEY - WATER YEARS 1933 THROUGH 1941

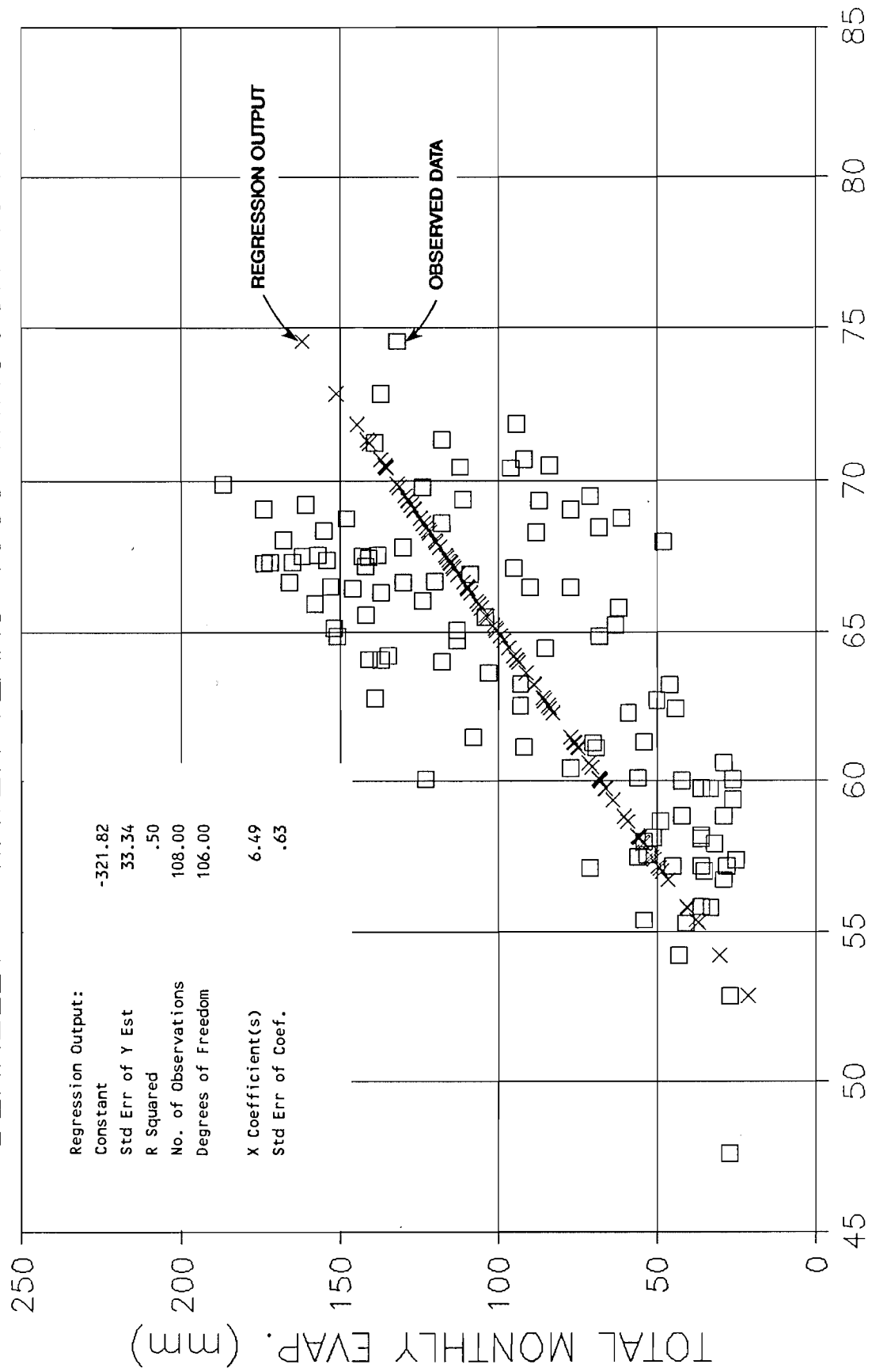
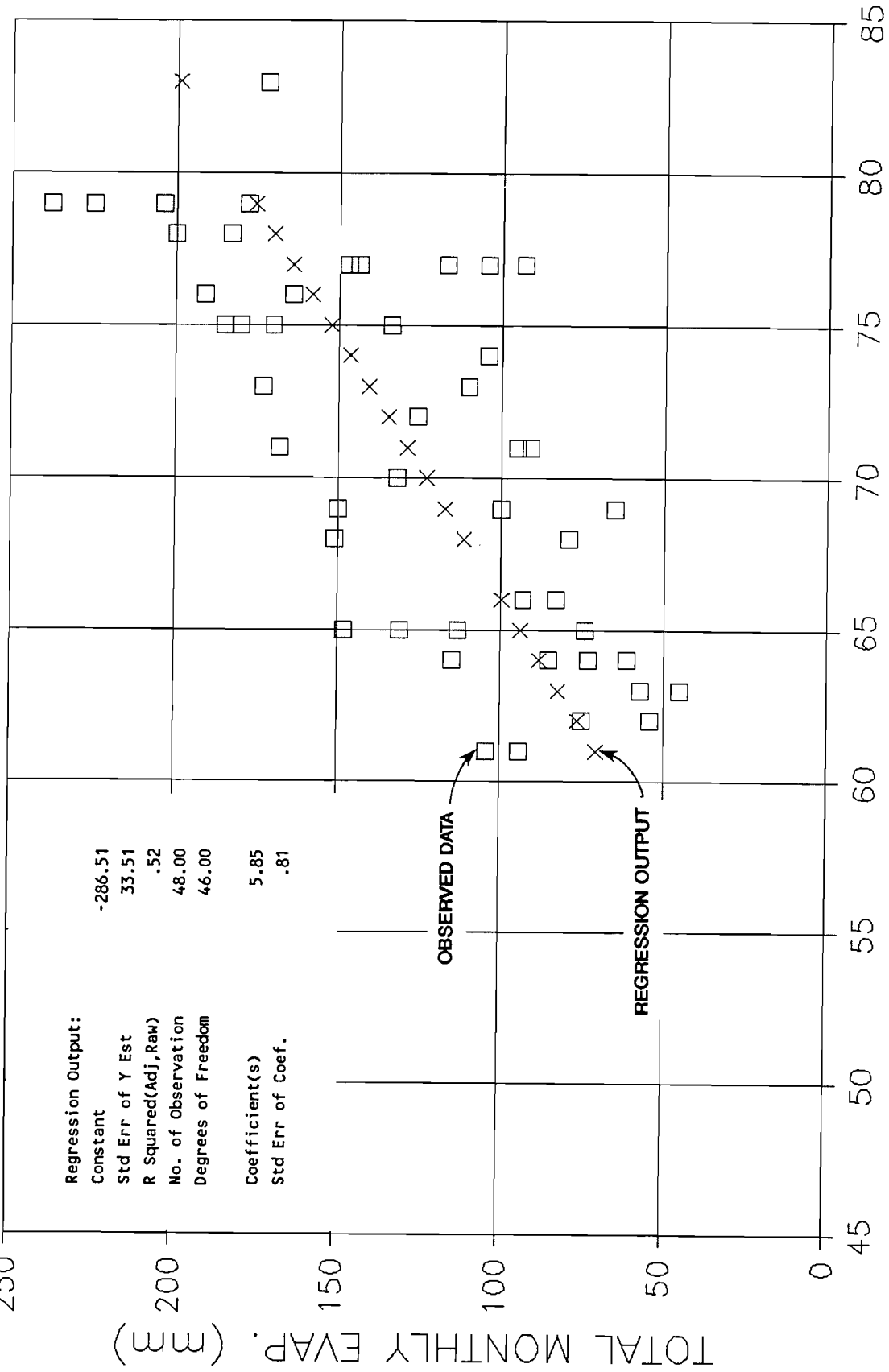


FIGURE 19

# EVAPORATION VS. TEMPERATURE

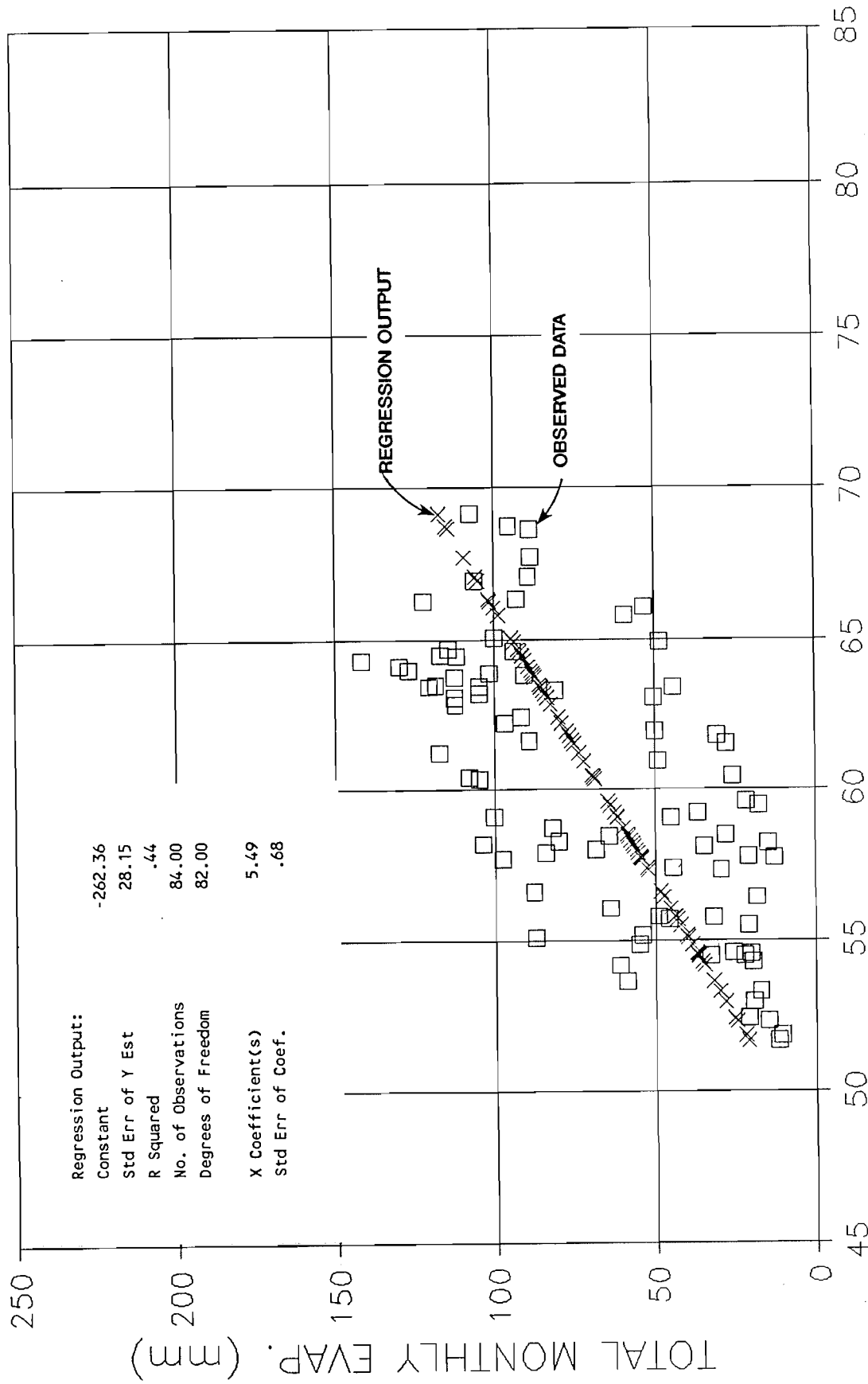
CAMP SAN LUIS OBISPO - WATER YEARS 1975 THROUGH 1978





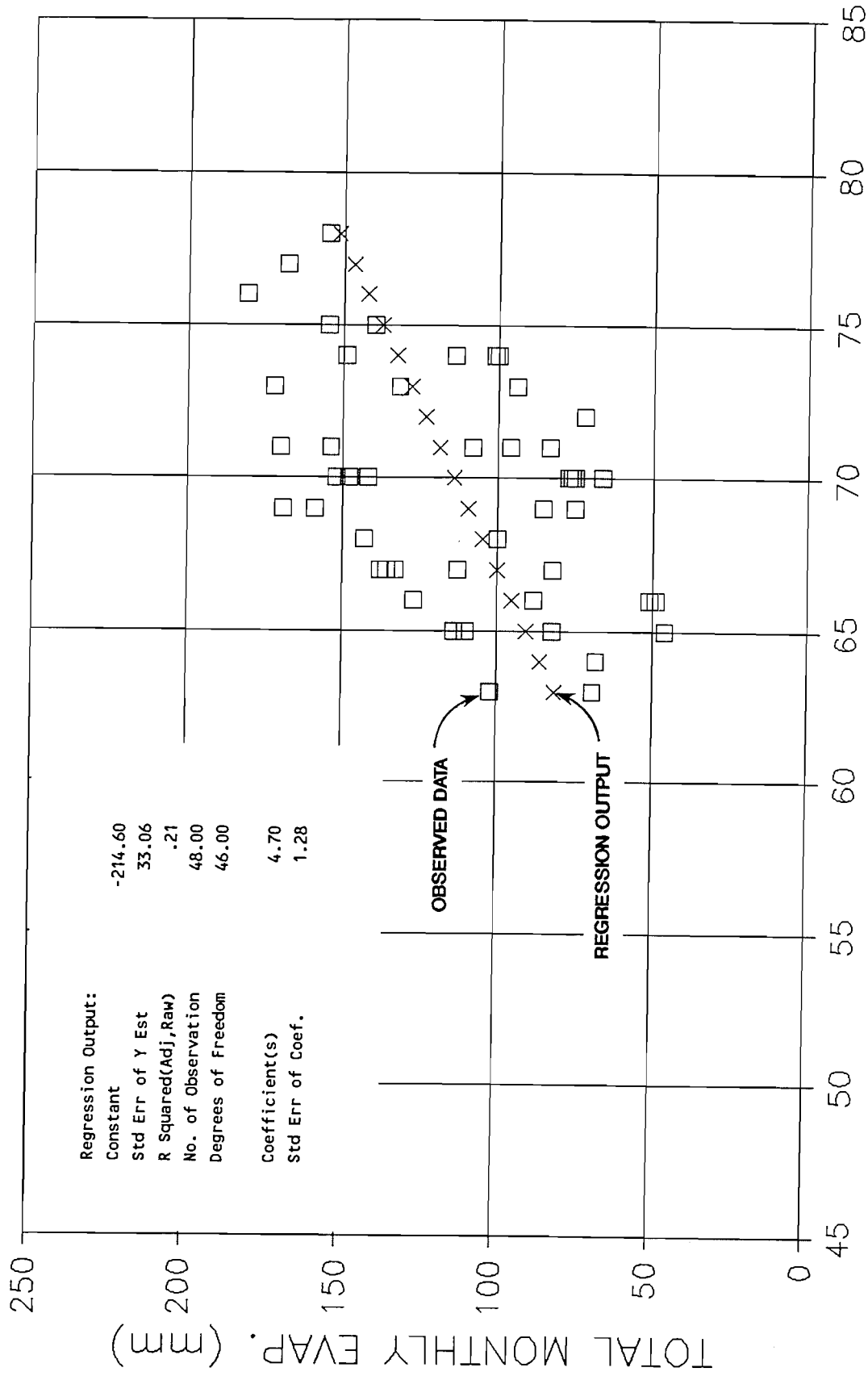
# EVAPORATION VS. TEMPERATURE

FERNDALDE - WATER YEARS '64, '66, '67, '69, '70, '71, '73



# EVAPORATION VS. TEMPERATURE

## OCEANO - WATER YEARS 1975 THROUGH 1978



AVG. MONTHLY MAX. TEMP. (degrees F)

# DRYDOCK GULCH AREA-CAPACITY CURVE

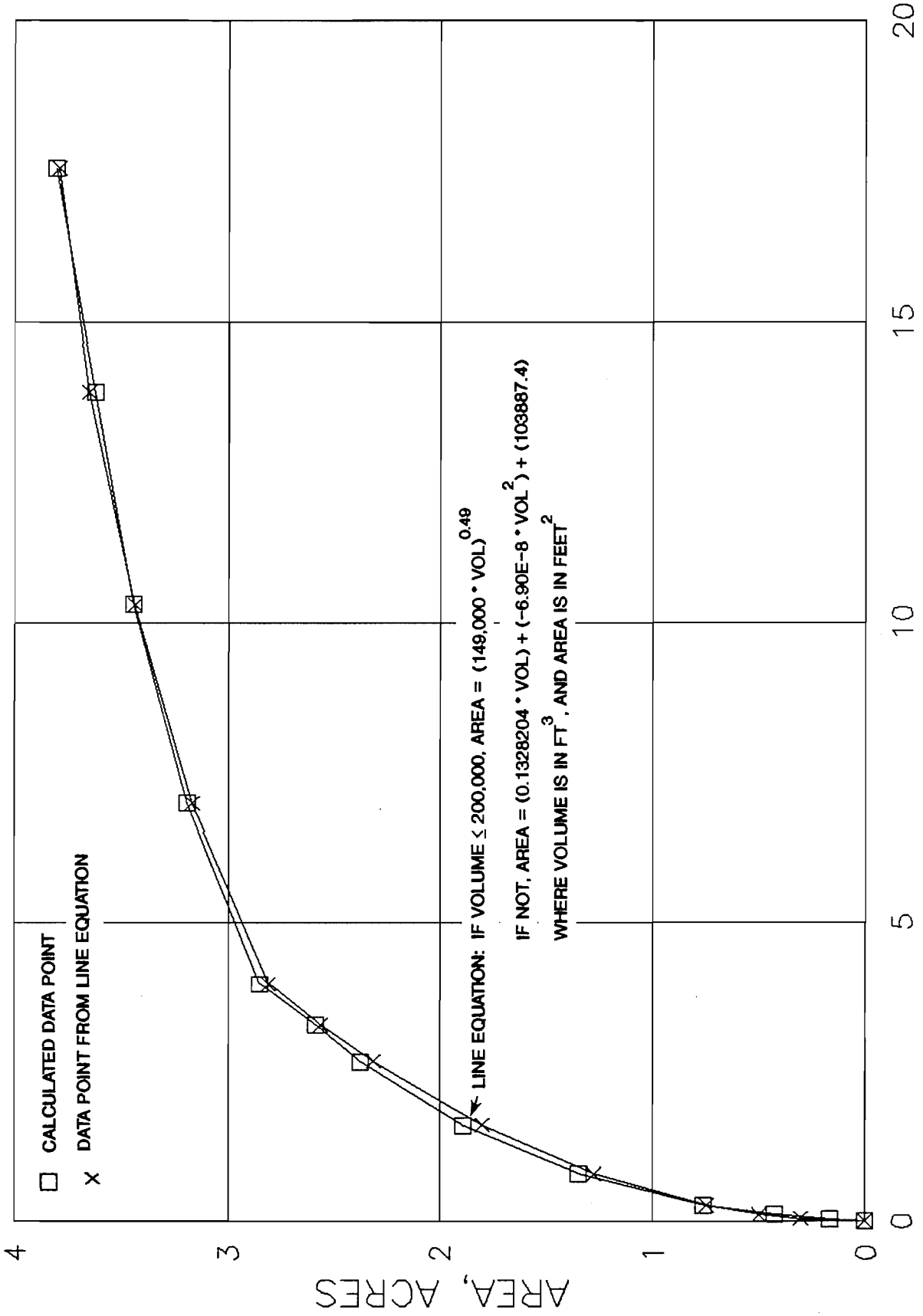


FIGURE 23

# DRYDOCK GULCH DEPTH-CAPACITY CURVE

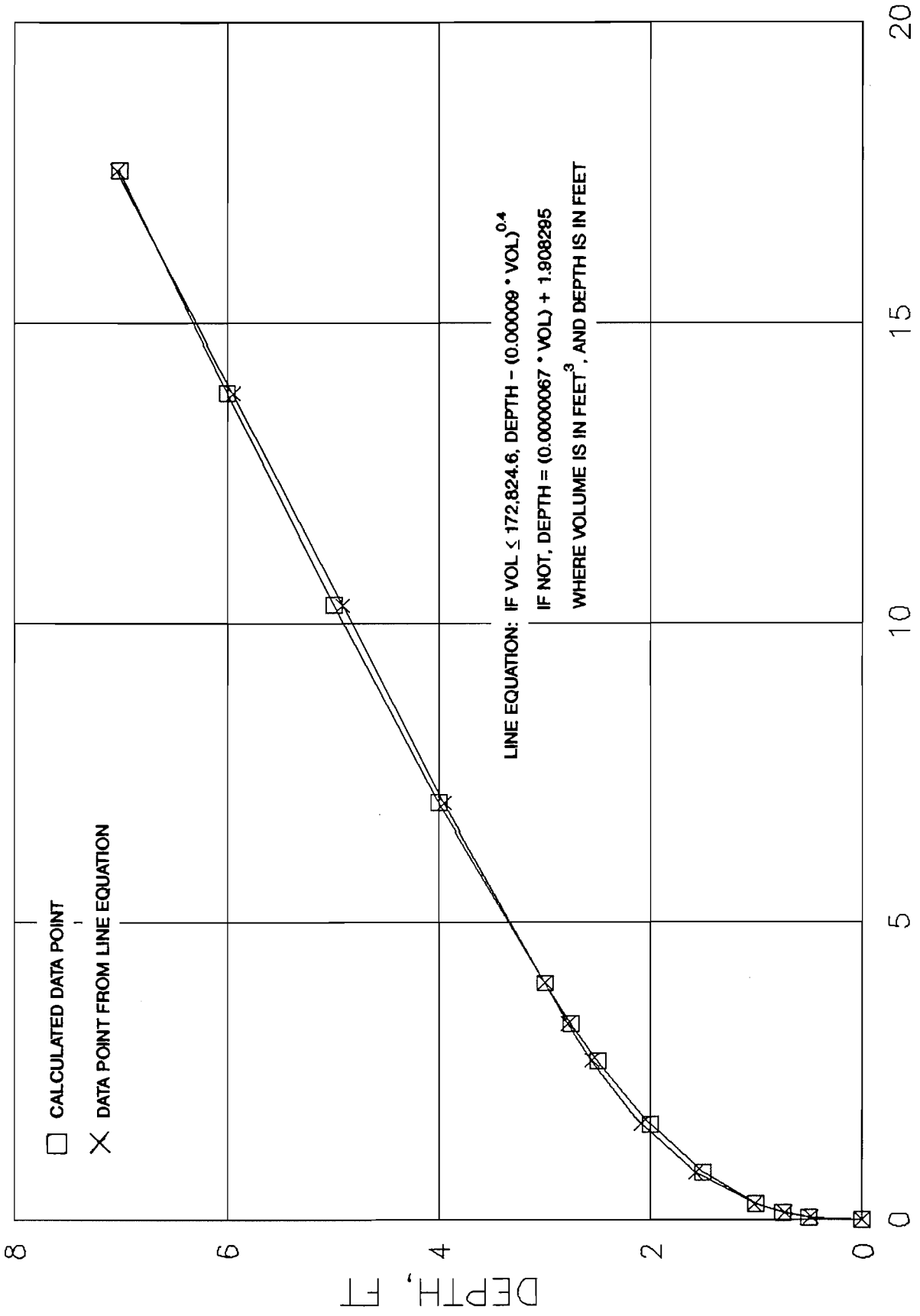
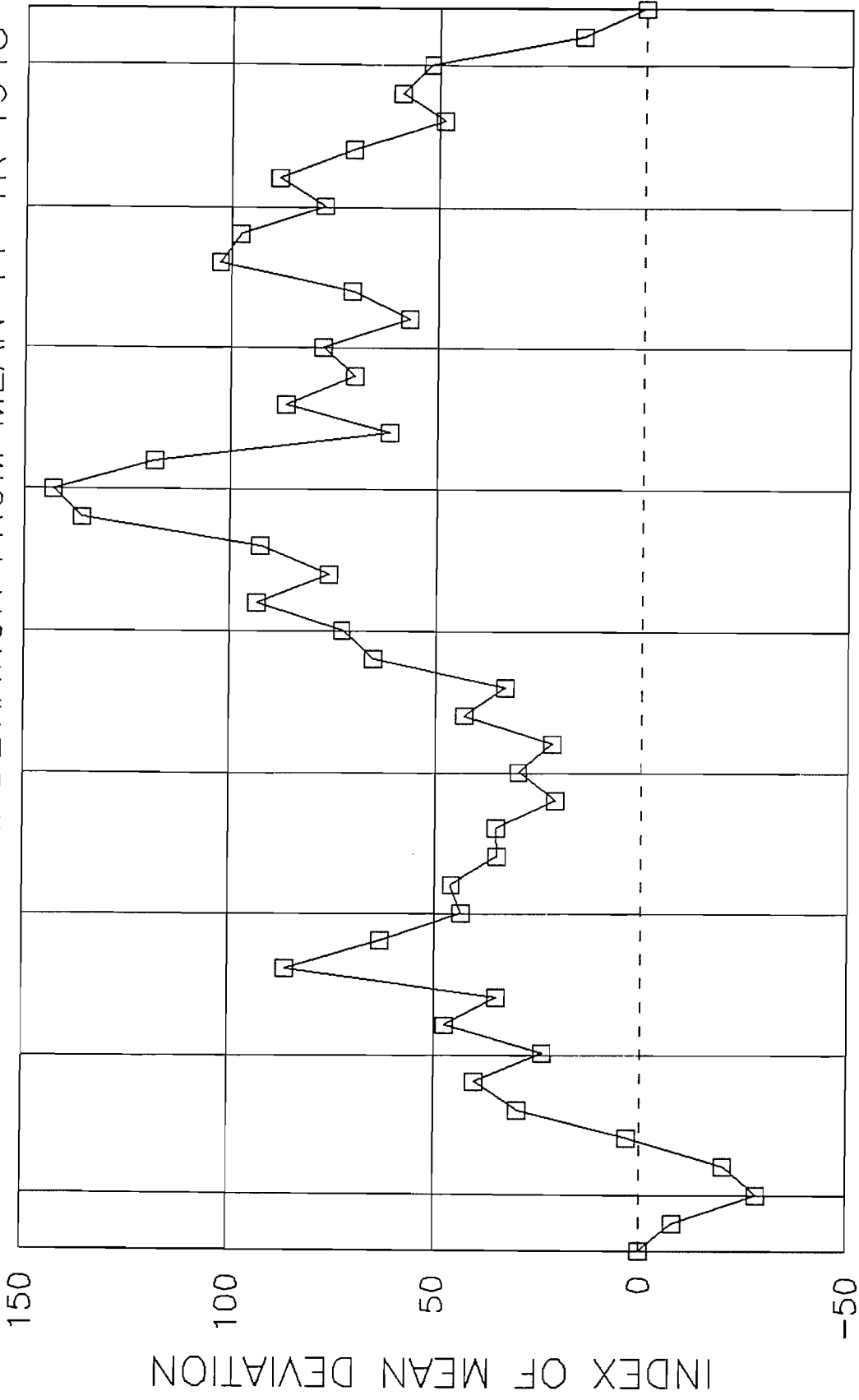


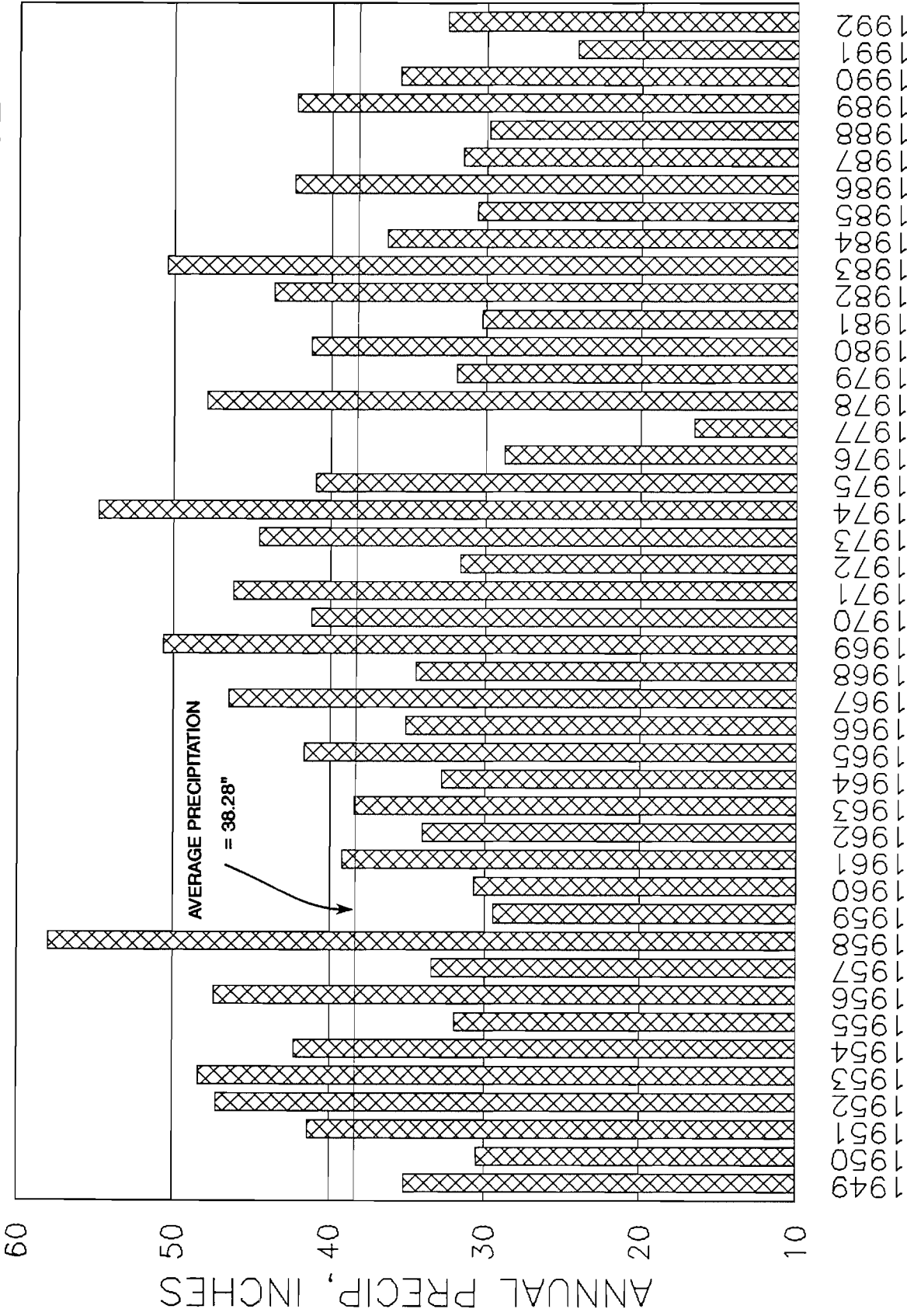
FIGURE 24

FT BRAGG PRECIP - CUM DEVIATION FROM MEAN 44-YR 1948-92



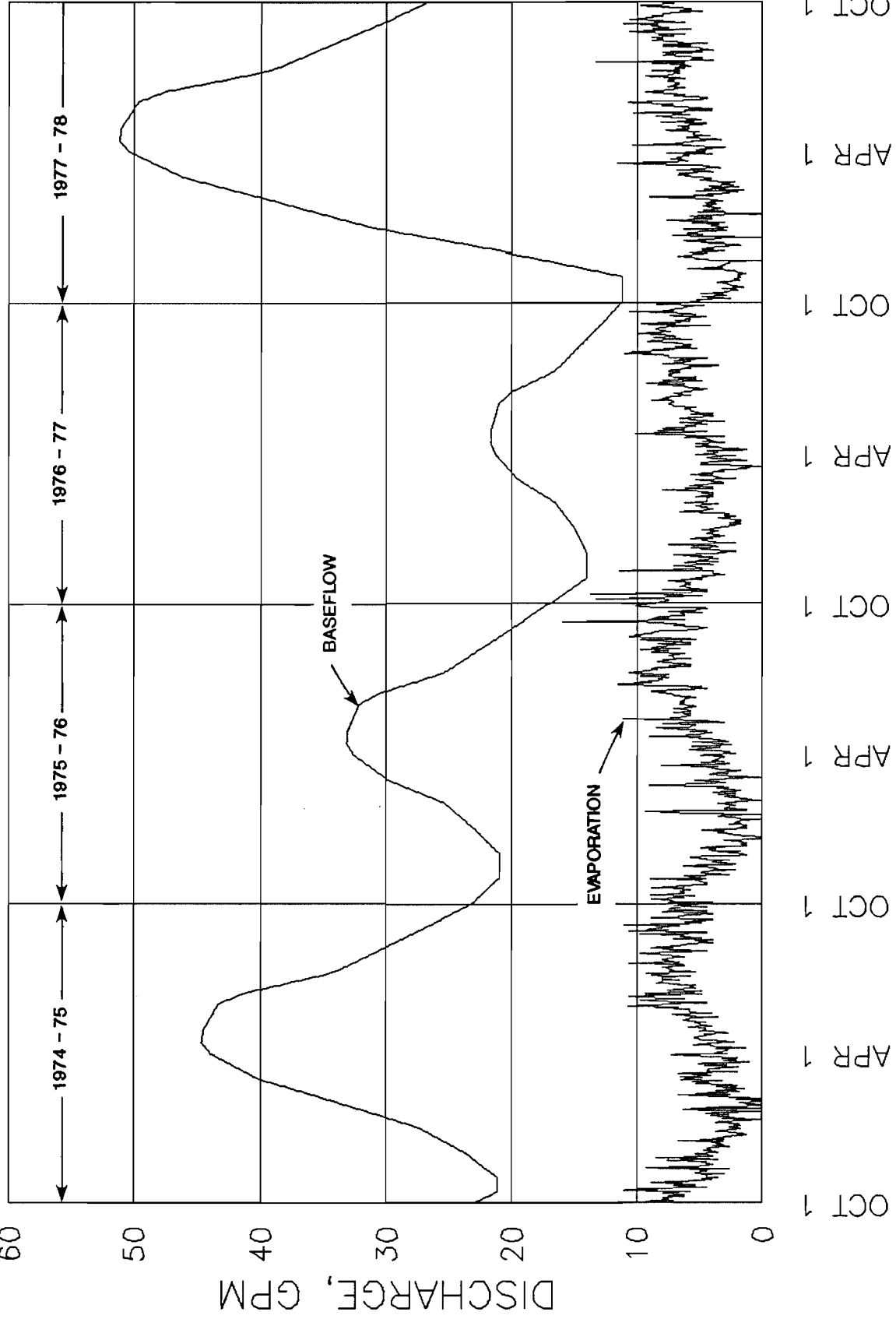
WATER YEAR ENDING SEPTEMBER 30

# FT BRAGG PRECIPITATION 44-YR PERIOD 1948-92



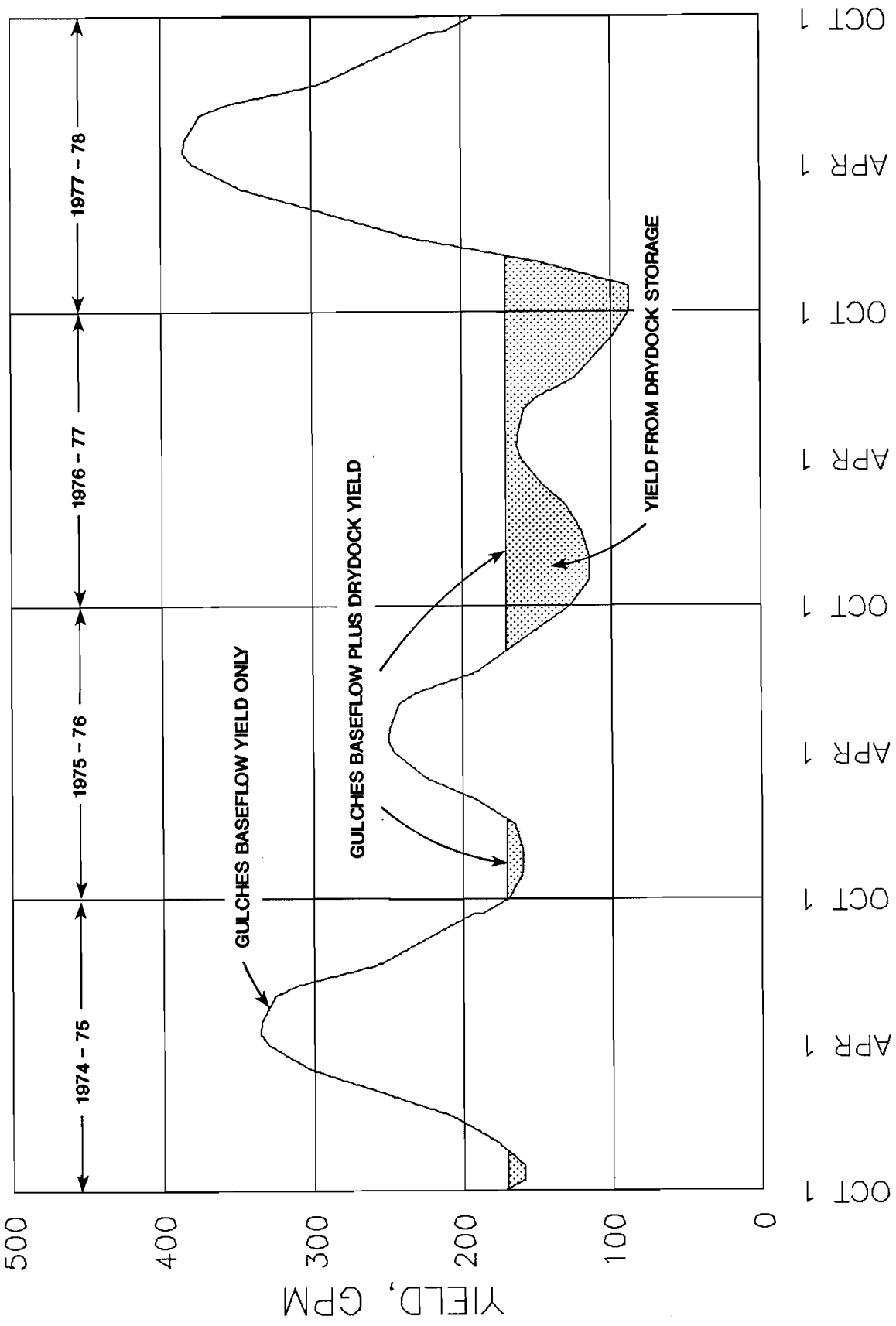
WATER YEAR ENDING SEPTEMBER 30

# DRYDOCK GULCH - BASEFLOW AND EVAPORATION 1974-78



DAILY TIME STEPS

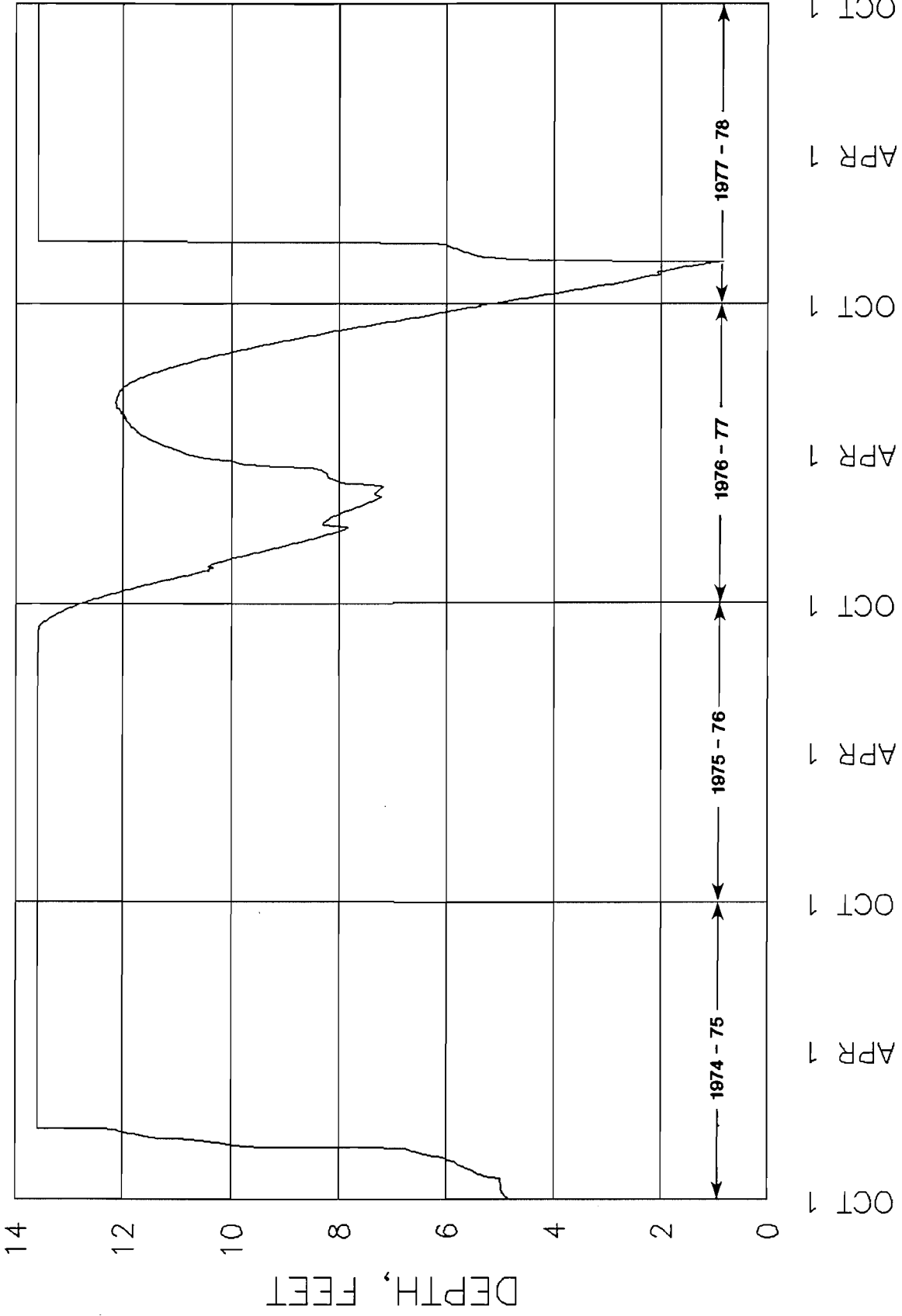
GULCHES + DRYDOCK YIELD - MAX CAP 40 AF, DEPTH 14 FT



DAILY TIME--STEPS

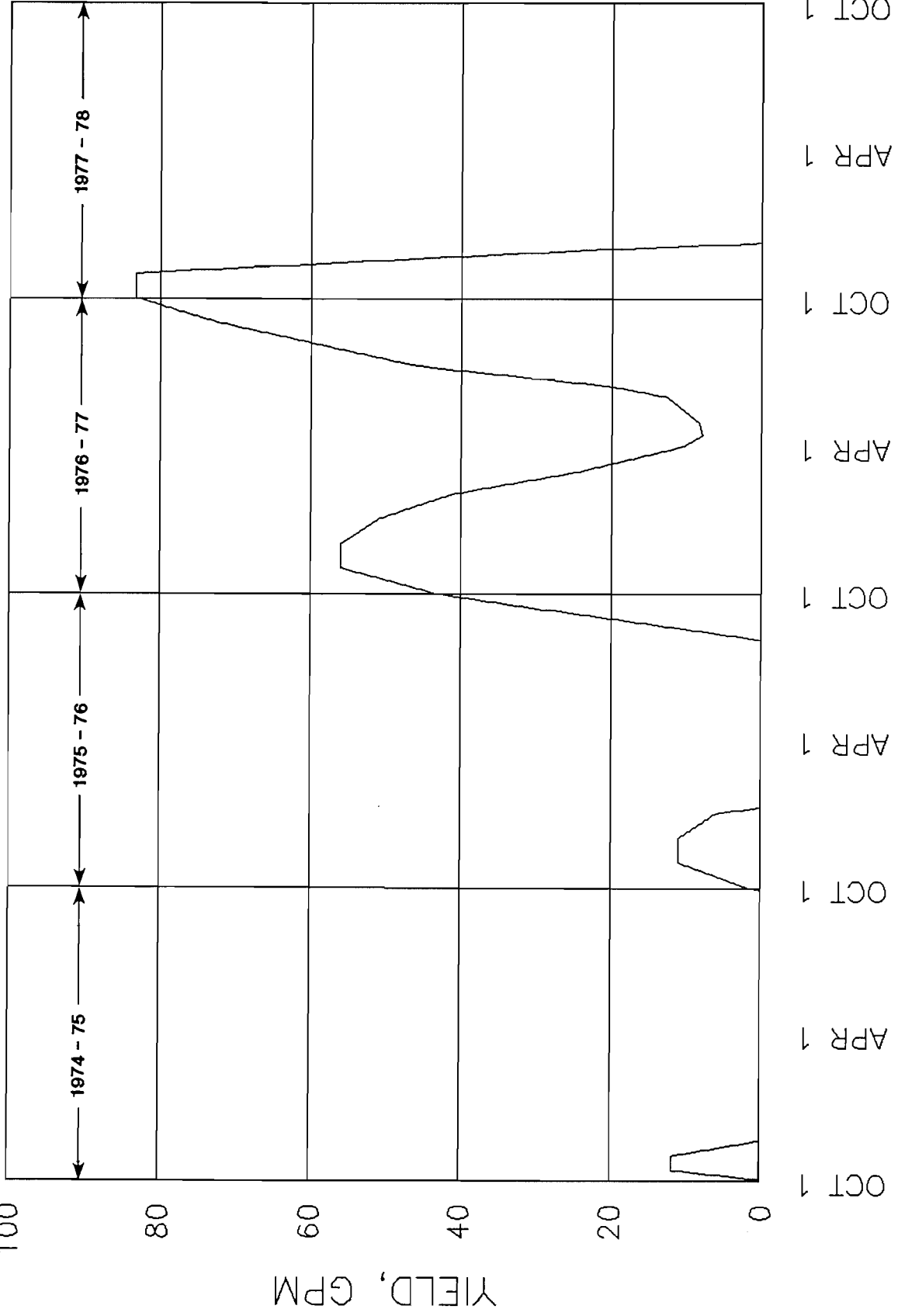


DRYDOCK RESERVOIR WATER LEVELS - MAX CAPACITY 40 AF



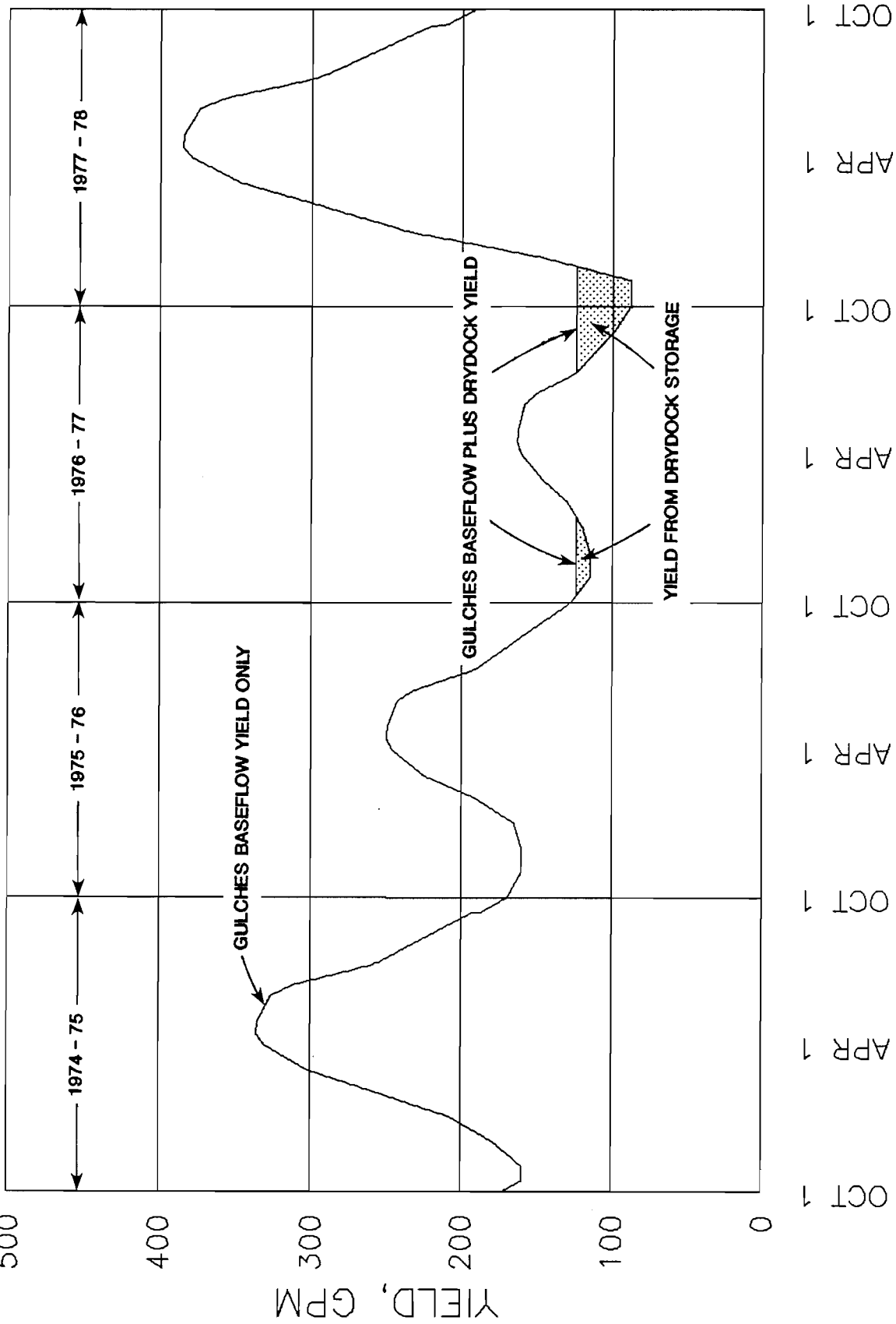
DAILY TIME-STEPS

DRYDOCK RESERVOIR YIELD - MAX CAPACITY 40 AF, DEPTH 14 FT



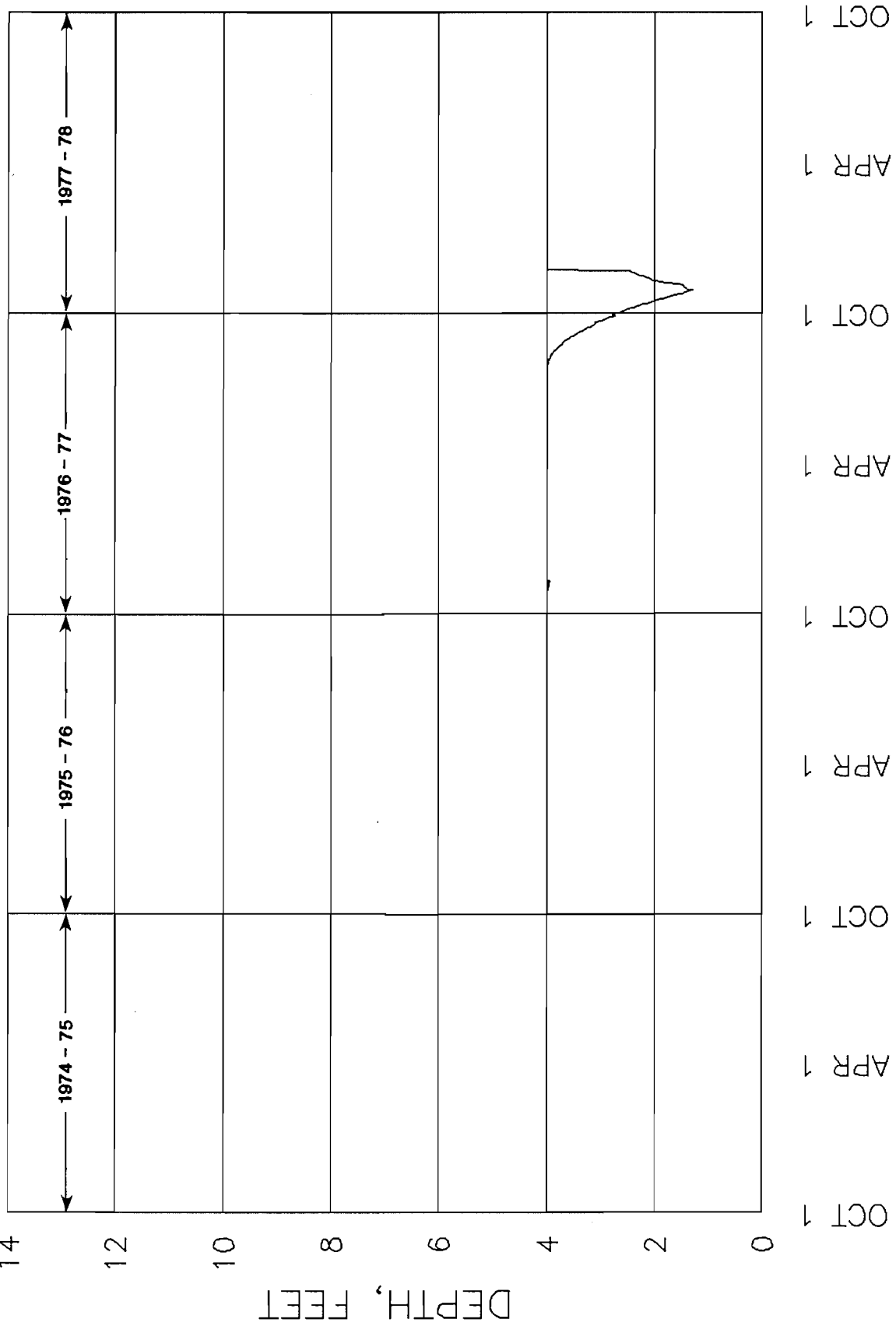
DAILY TIME-STEPS

GULCHES + DRYDOCK YIELD - MAX CAP 7.2 AF, DEPTH 4 FT



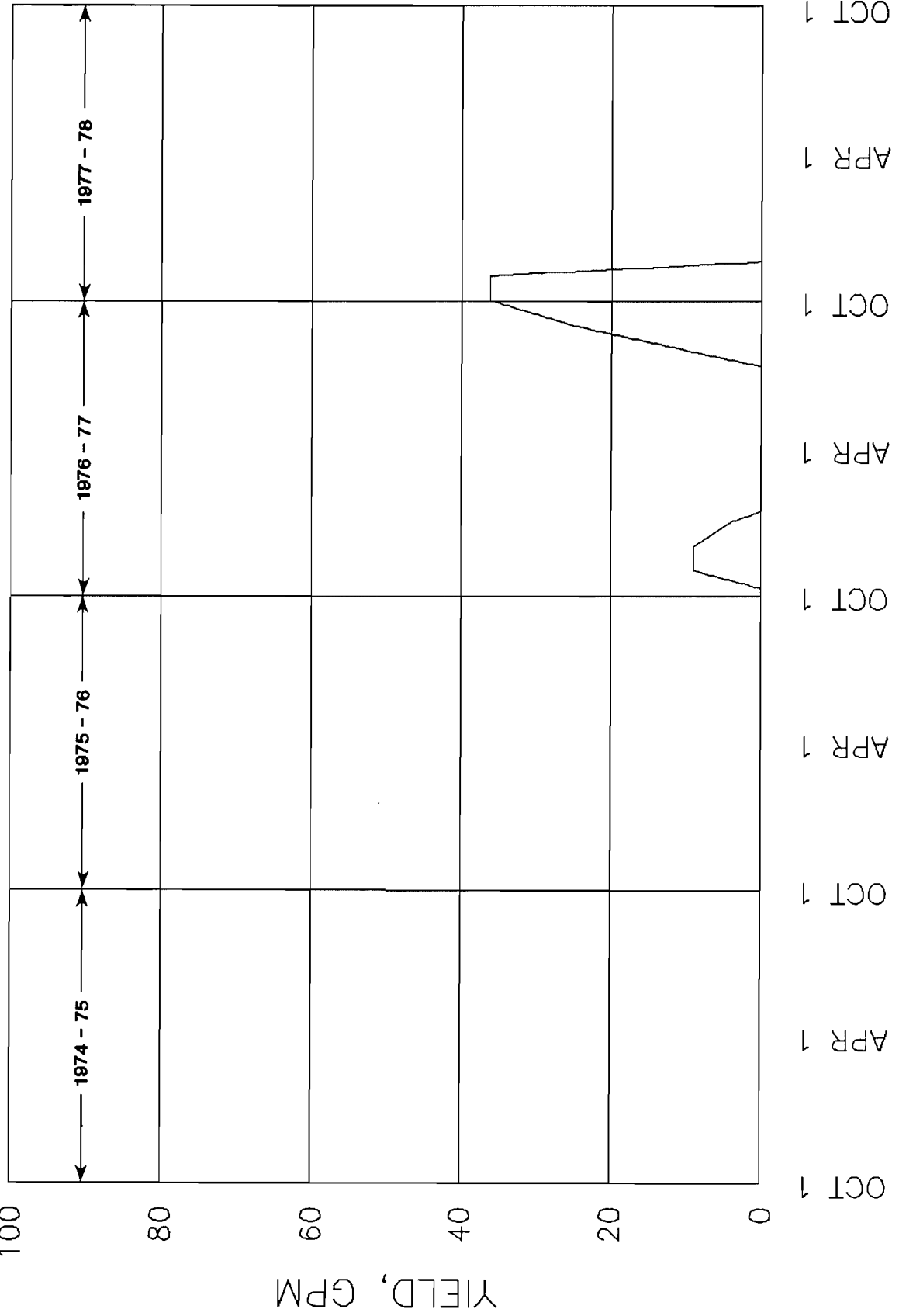
DAILY TIME-STEPS

DRYDOCK RESERVOIR WATER LEVELS - MAX CAPACITY 7.2 AF



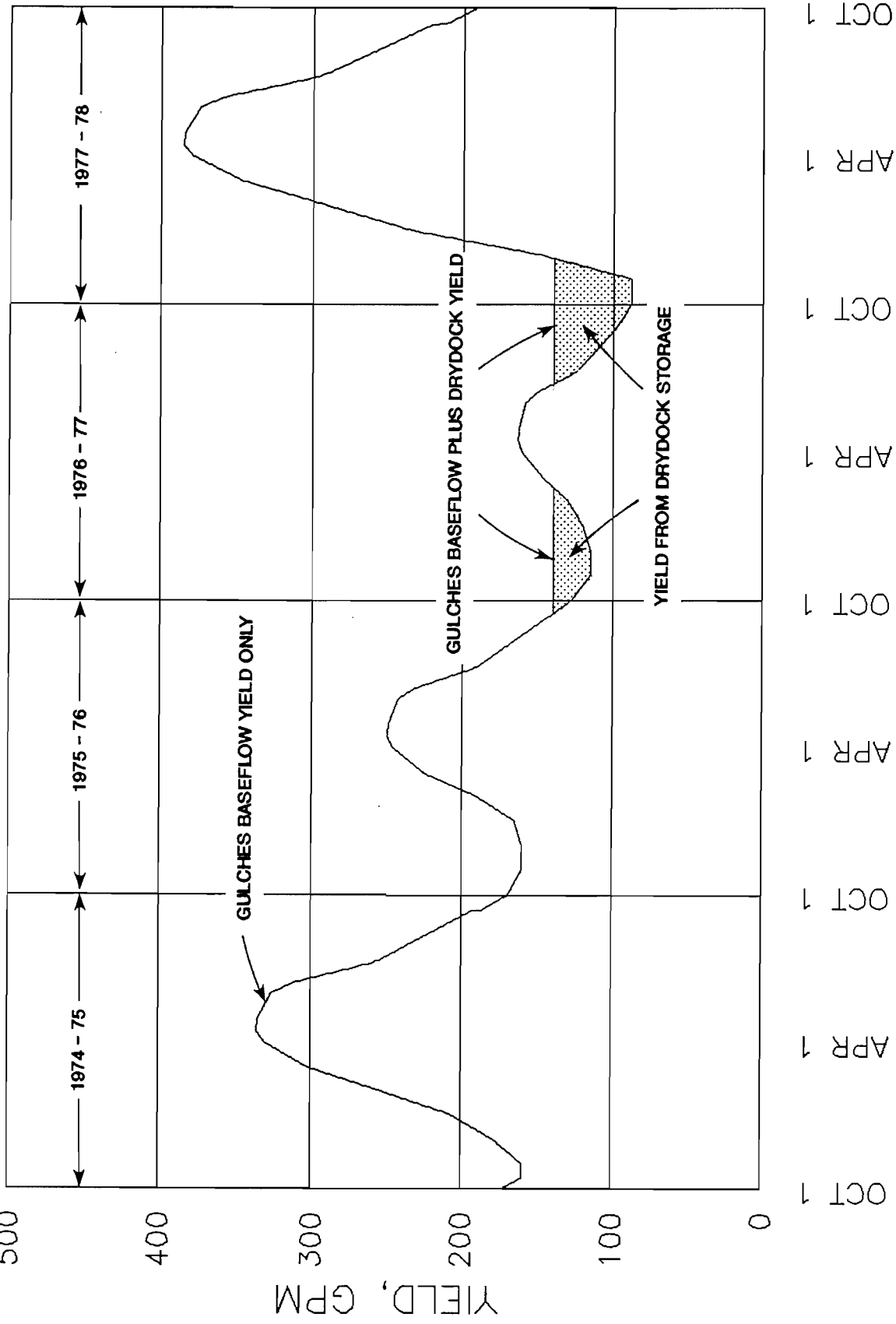
DAILY TIME-STEPS

DRYDOCK RESERVOIR YIELD -- MAX CAPACITY 7.2 AF, DEPTH 4 FT



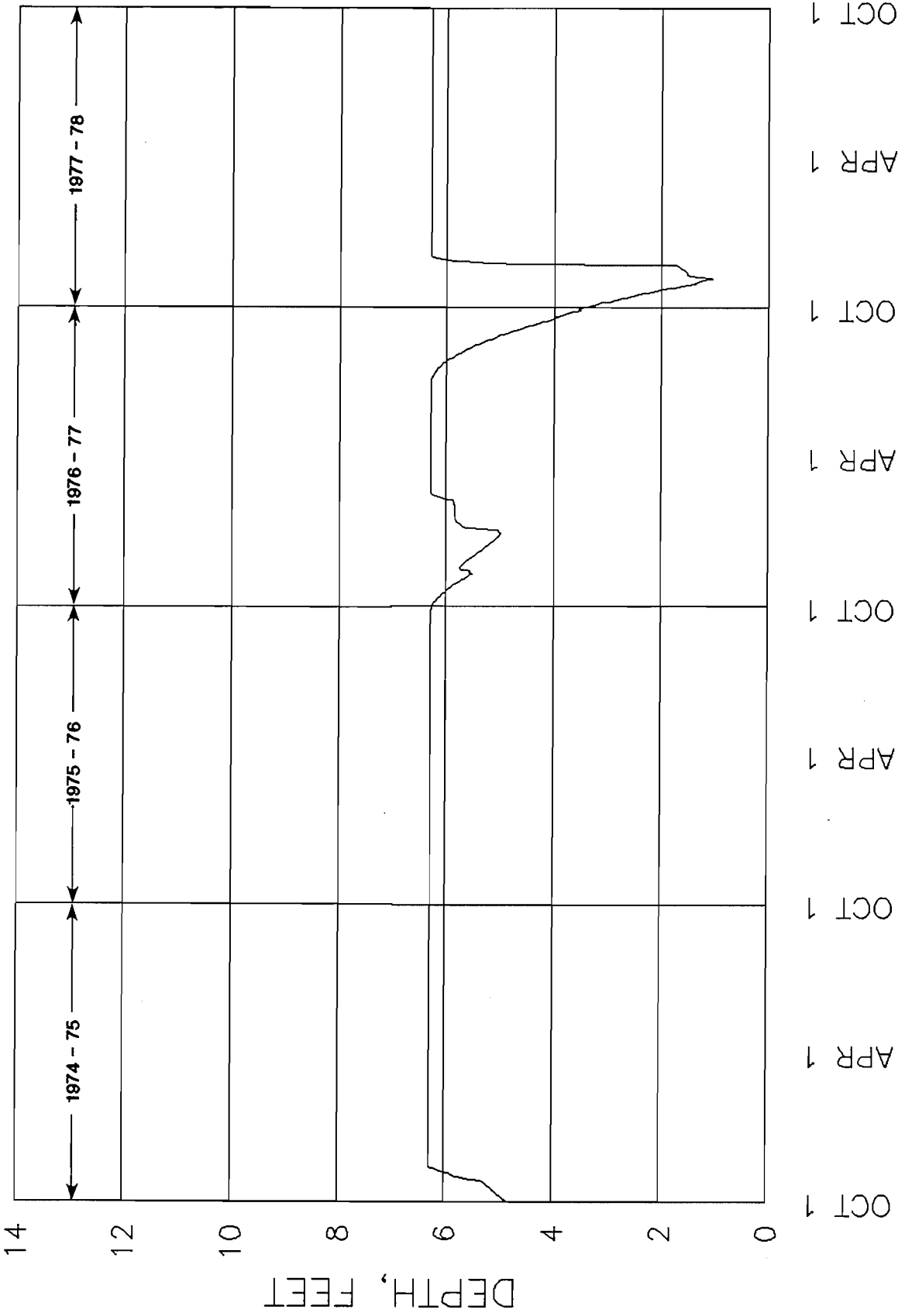
DAILY TIME--STEPS

GULCHES + DRYDOCK YIELD - MAX CAP 15 AF, DEPTH 6 FT



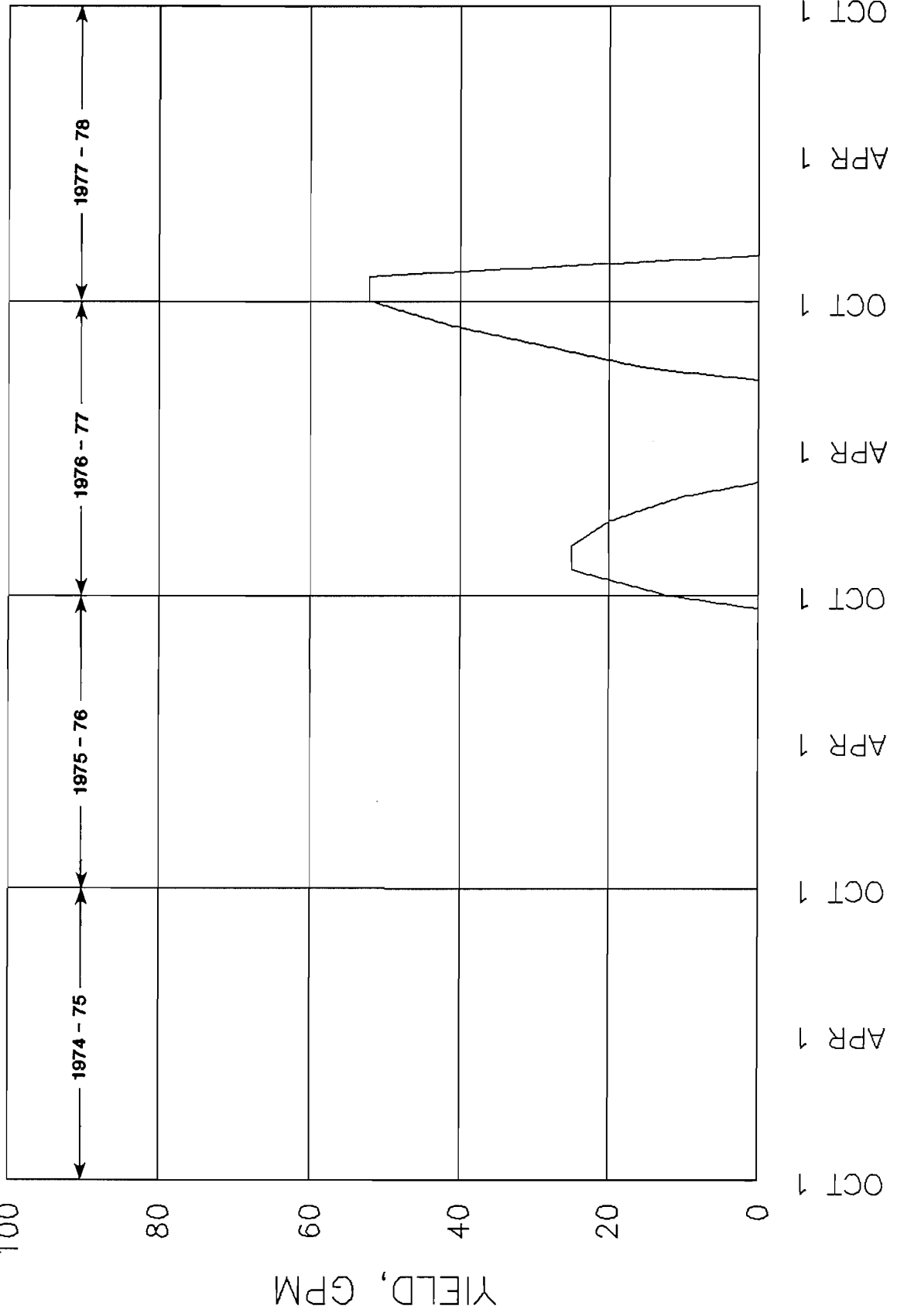
DAILY TIME-STEPS

DRYDOCK RESERVOIR WATER LEVELS - MAX CAPACITY 15 AF



DAILY TIME--STEPS

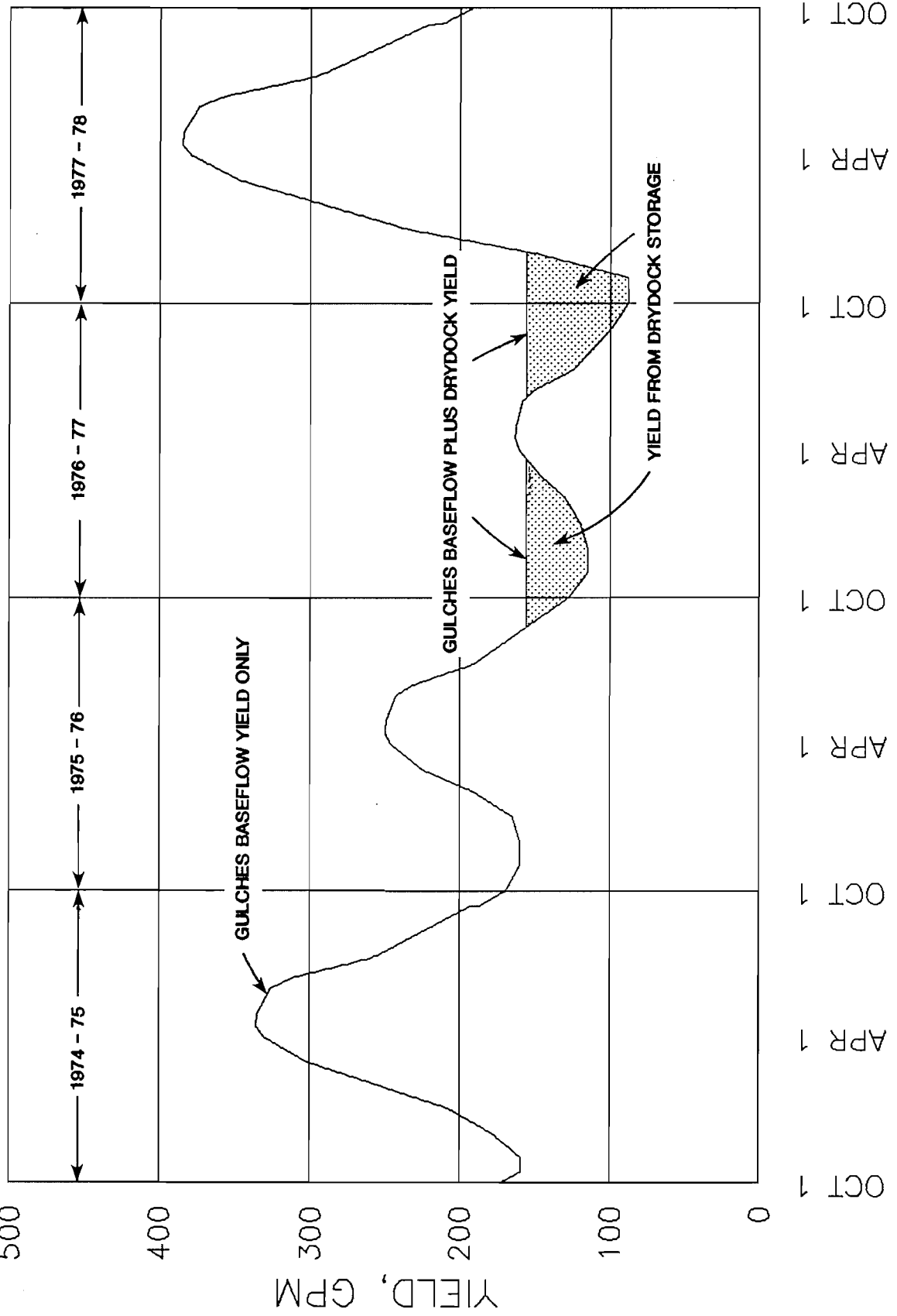
DRYDOCK RESERVOIR YIELD - MAX CAPACITY 15 AF, DEPTH 6 FT



DAILY TIME-STEPS

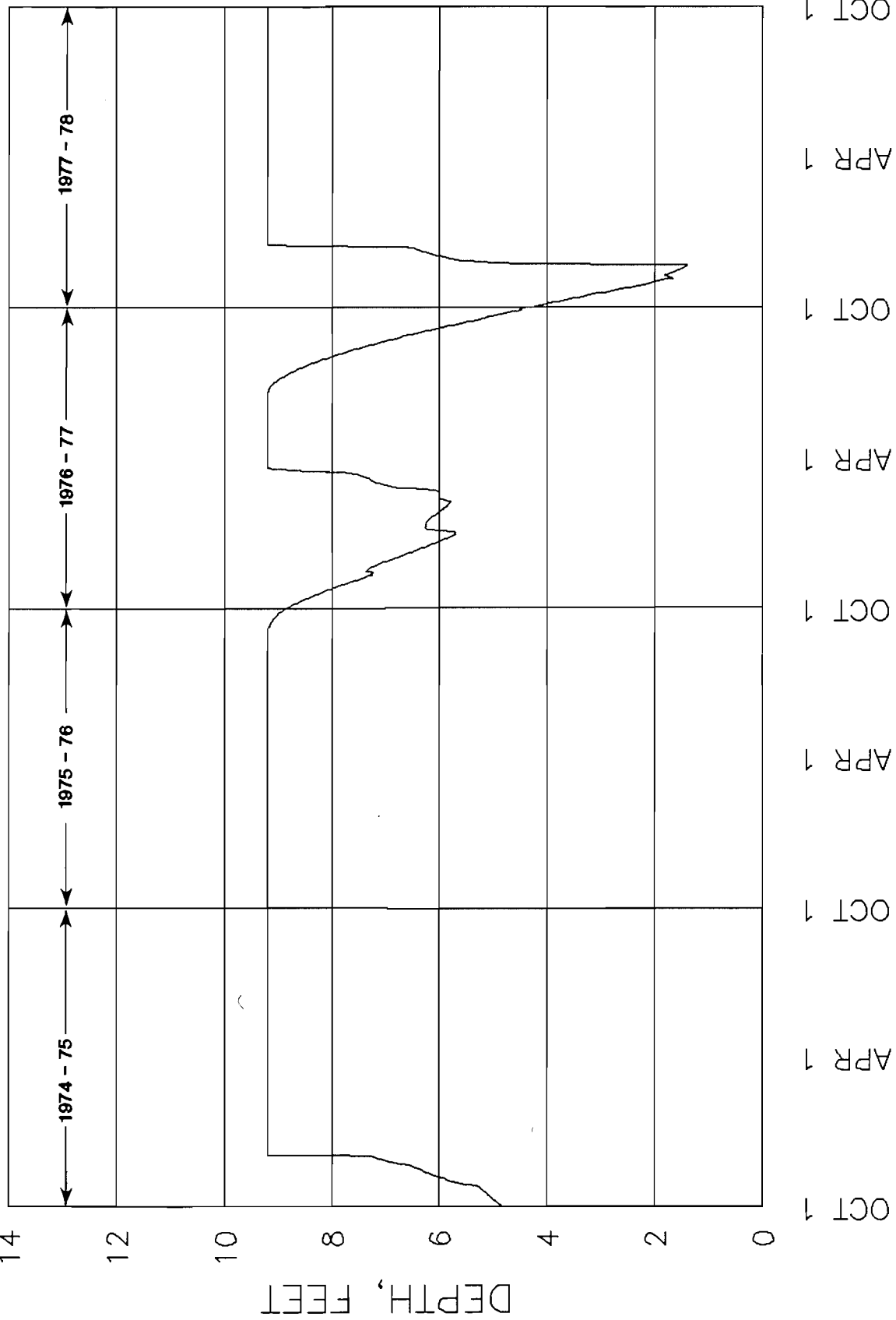


GULCHES + DRYDOCK YIELD - MAX CAP 25 AF, DEPTH 9 FT



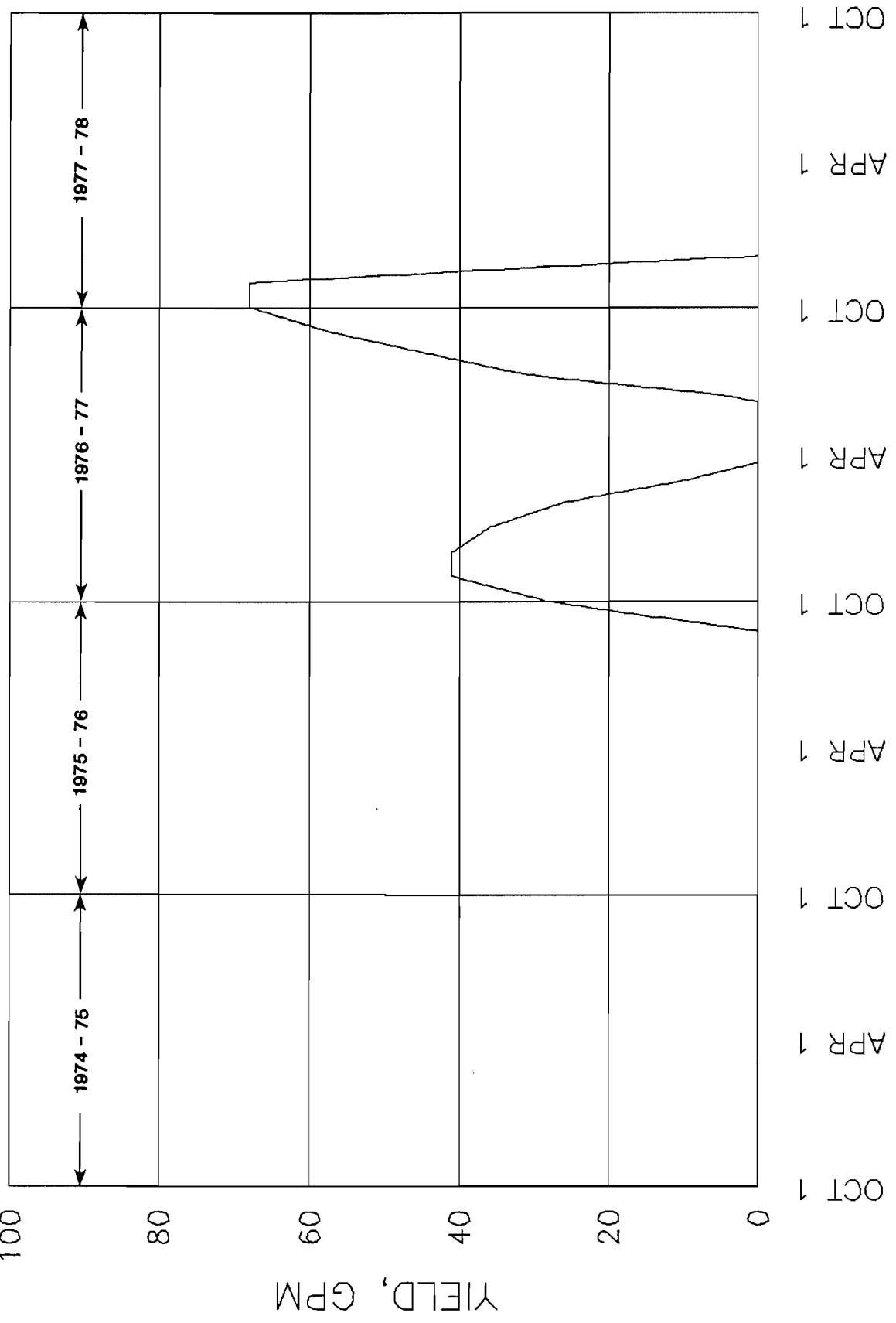
DAILY TIME-STEPS

DRYDOCK RESERVOIR WATER LEVELS - MAX CAPACITY 25 AF



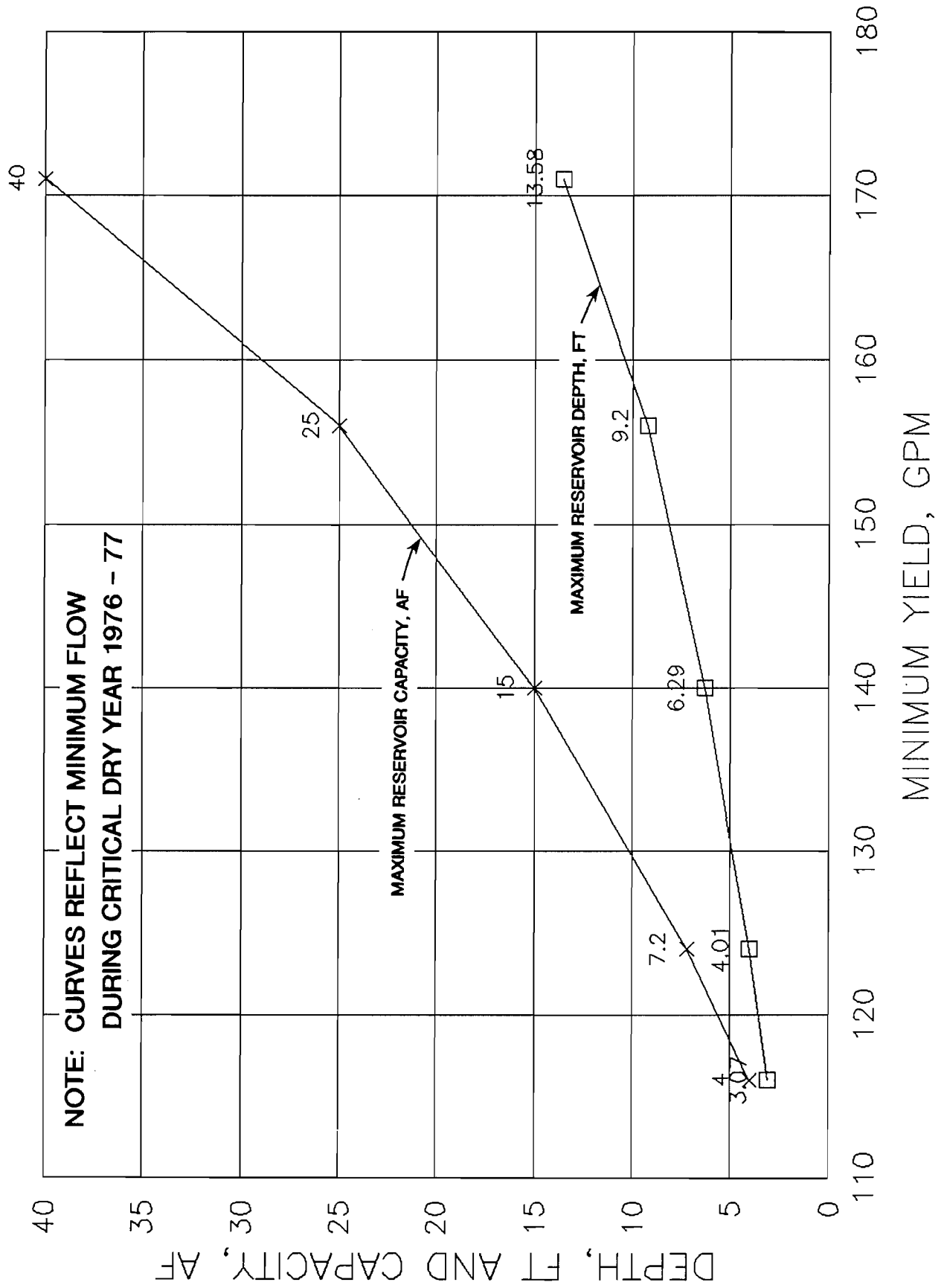
DAILY TIME-STEPS

DRYDOCK RESERVOIR YIELD - MAX CAPACITY 25 AF, DEPTH 9 FT

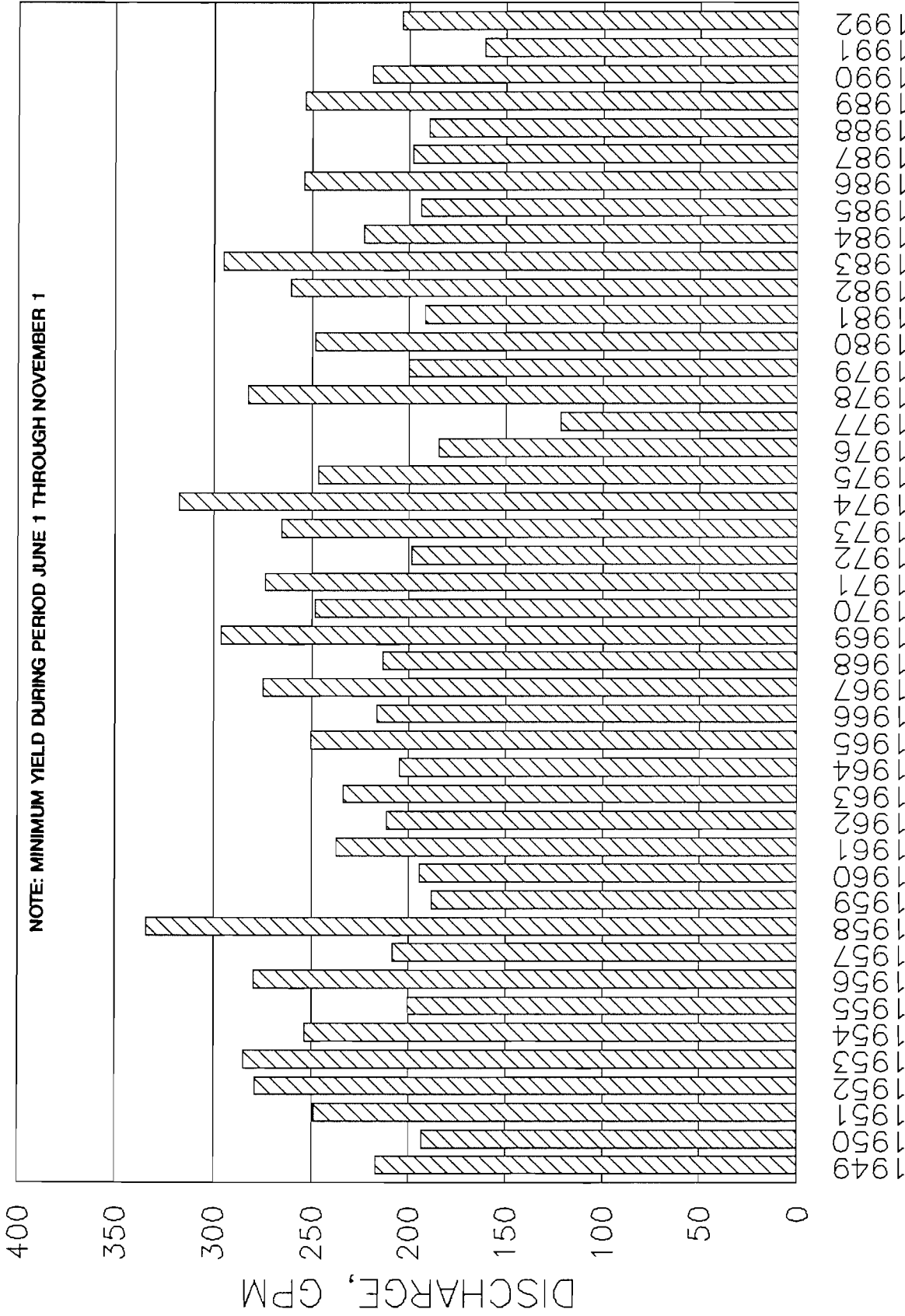


DAILY TIME-STEPS

# DRYDOCK GULCH YIELD VS DEPTH AND CAPACITY, OP STUDY 1974-78

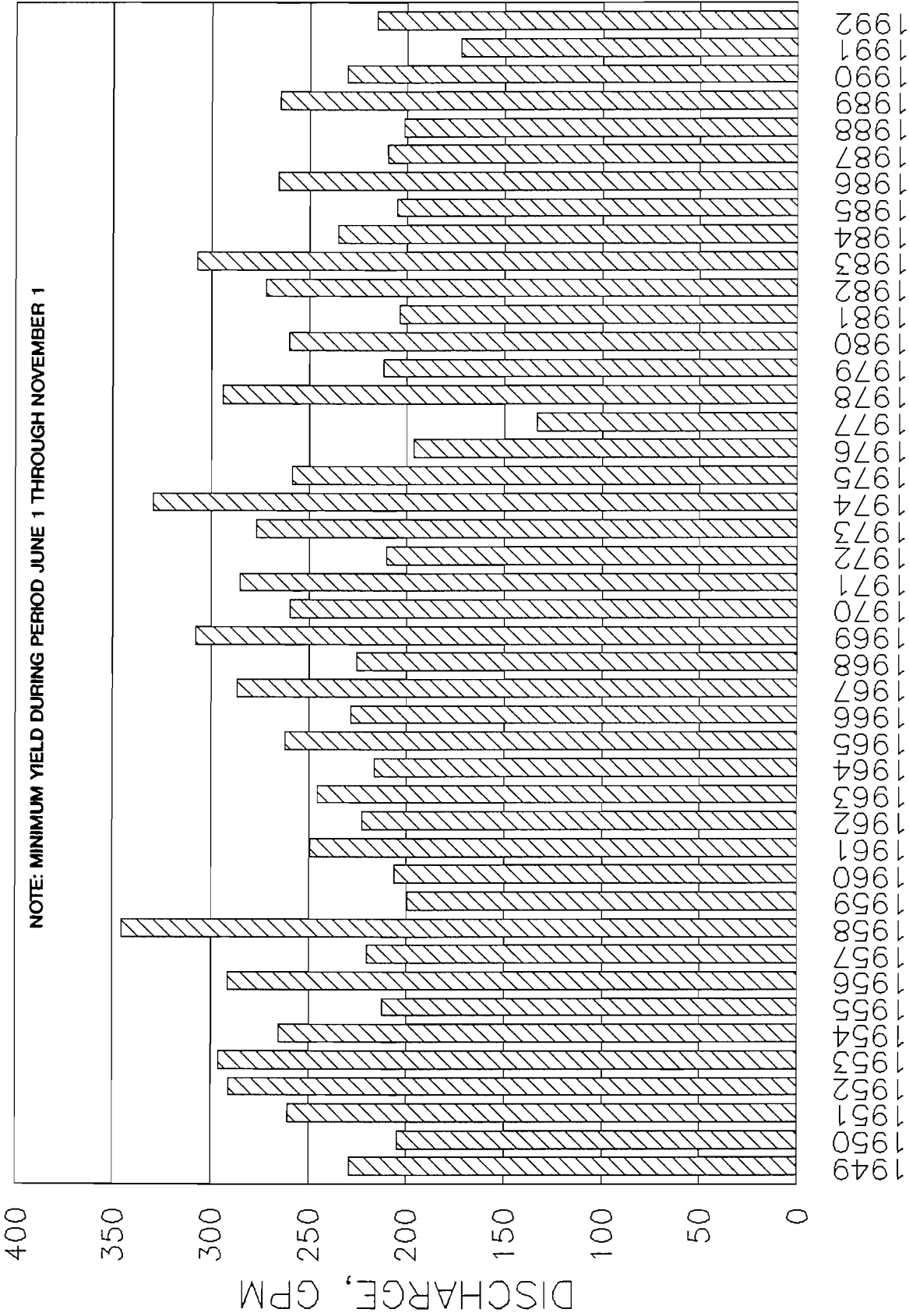


LOWER GULCHES + DRYDOCK MINIMUM SUMMER YIELD, RES 7.2 AF, DEPTH 4 FT



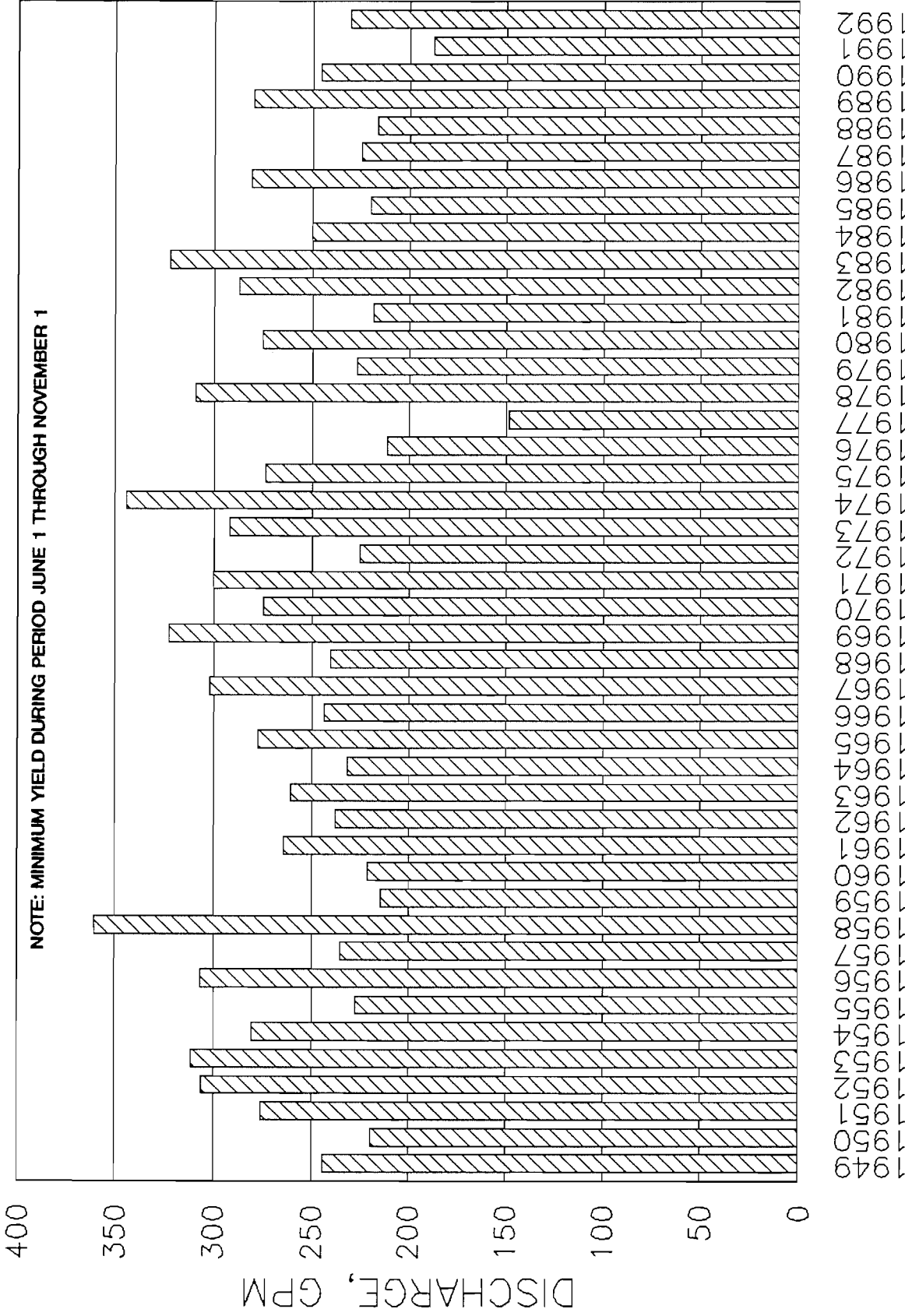
WATER YEAR ENDING SEPTEMBER 30

LOWER GULCHES + DRYDOCK MINIMUM SUMMER YIELD, RES 15 AF, DEPTH 6 FT



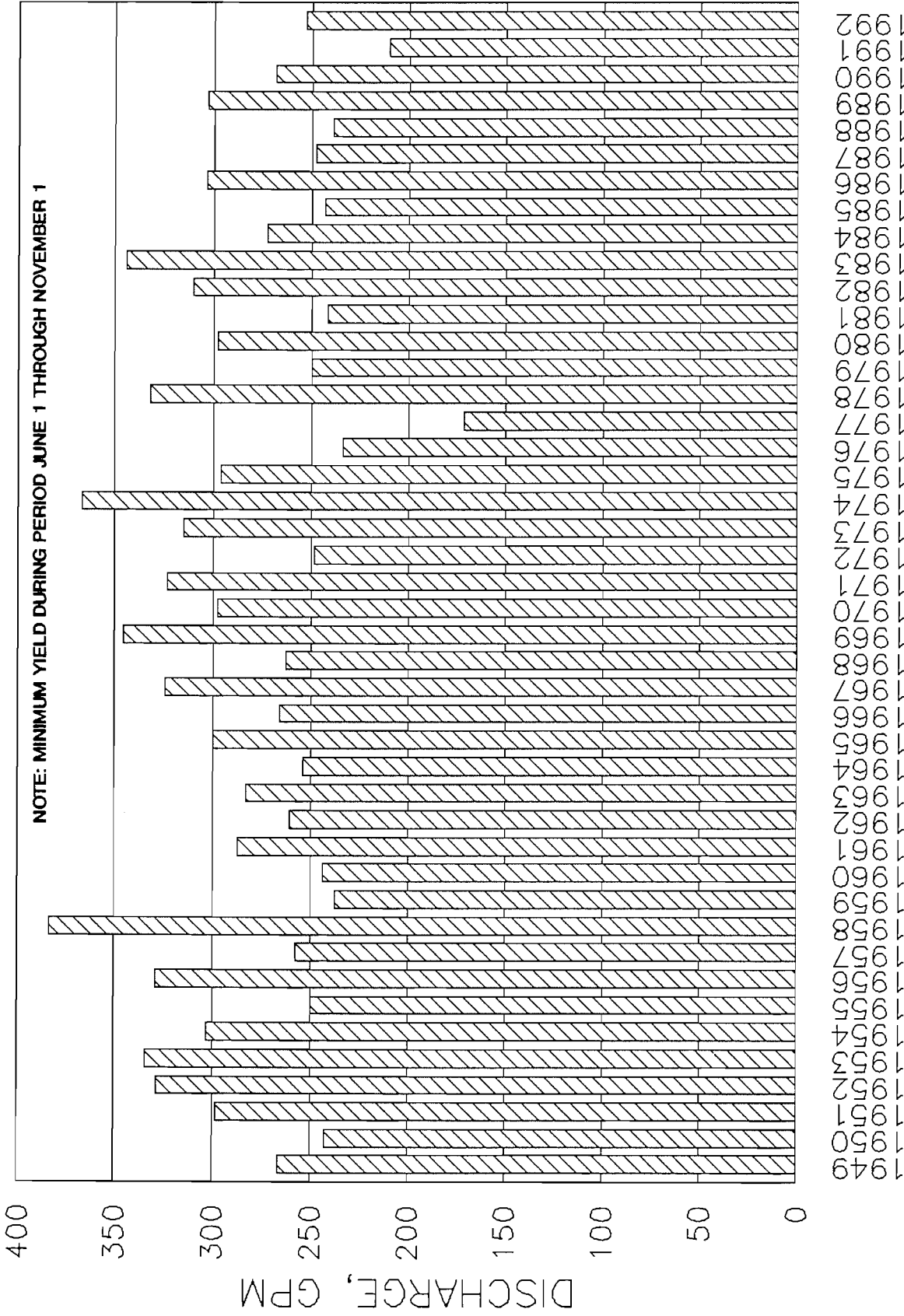
WATER YEAR ENDING SEPTEMBER 30

LOWER GULCHES + DRYDOCK MINIMUM SUMMER YIELD, RES 25 AF, DEPTH 9 FT



WATER YEAR ENDING SEPTEMBER 30

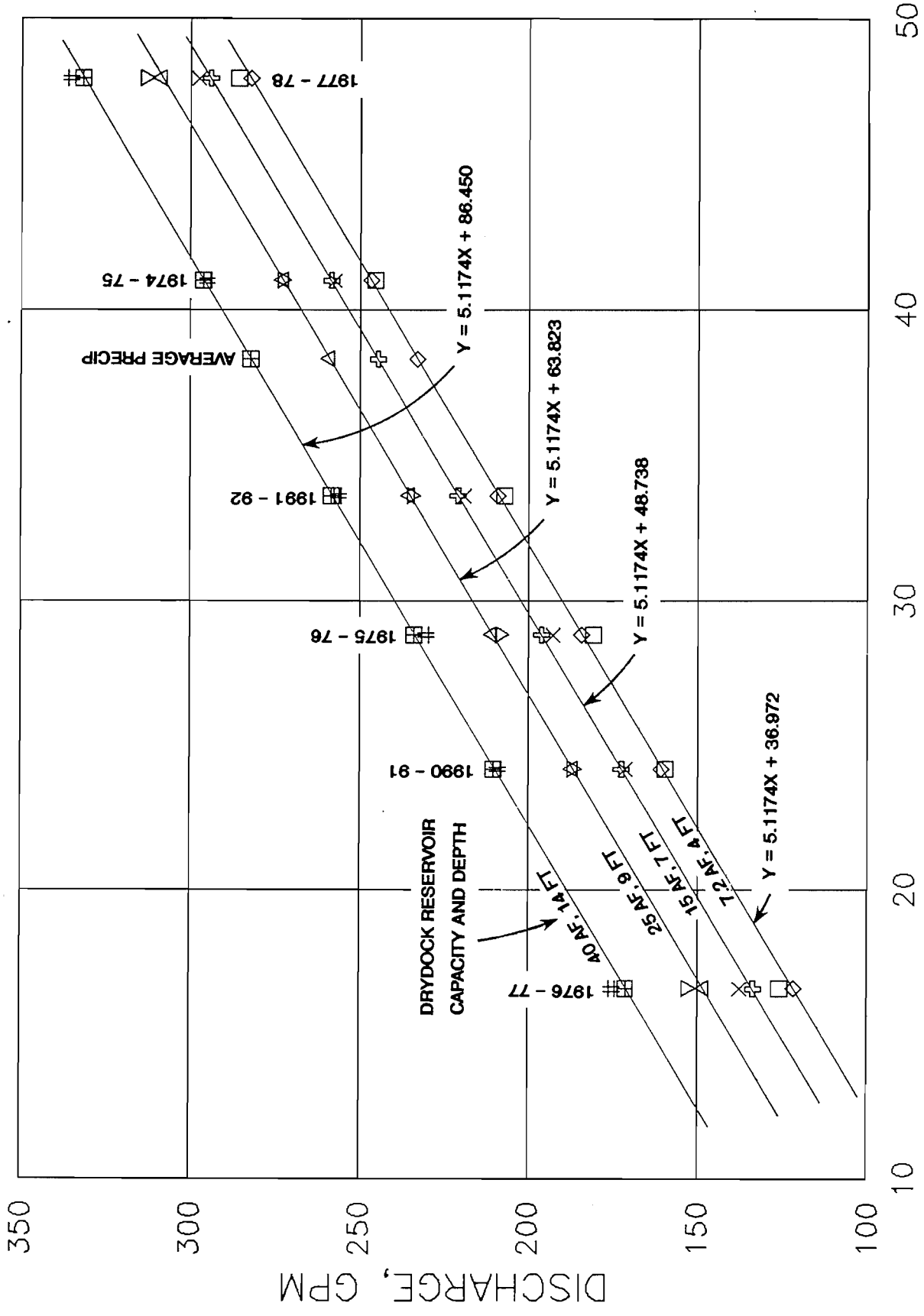
LOWER GULCHES + DRYDOCK MINIMUM SUMMER YIELD, RES 40 AF, DEPTH 14 FT



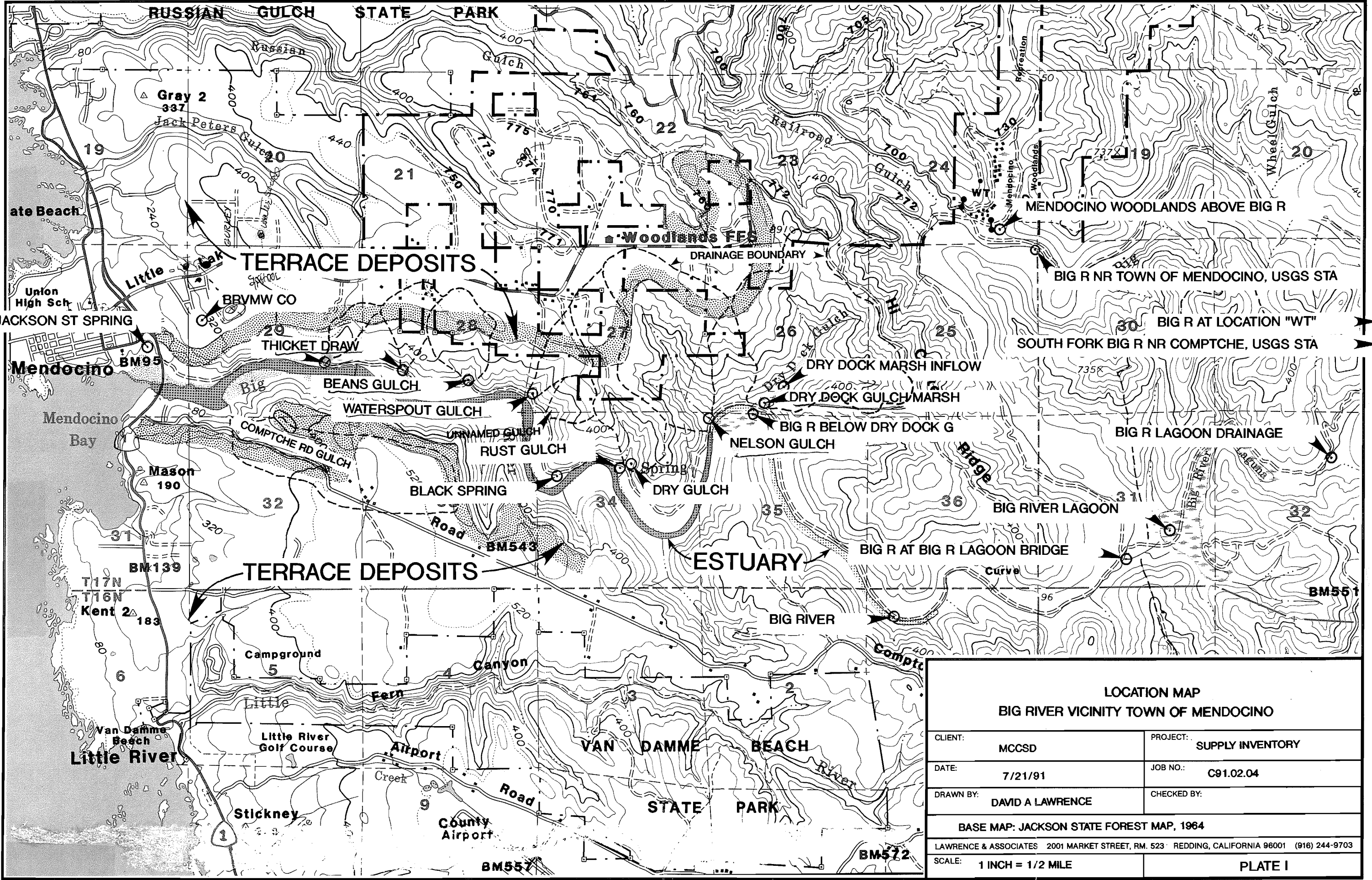
WATER YEAR ENDING SEPTEMBER 30



LOWER GULCHES + DRYDOCK MINIMUM SUMMER YIELD (JUN 1 TO NOV 1) VS PRECIP



FT BRAGG RAINFALL, INCHES



LOCATION MAP	
BIG RIVER VICINITY TOWN OF MENDOCINO	
CLIENT: MCCSD	PROJECT: SUPPLY INVENTORY
DATE: 7/21/91	JOB NO.: C91.02.04
DRAWN BY: DAVID A LAWRENCE	CHECKED BY:
BASE MAP: JACKSON STATE FOREST MAP, 1964	
LAWRENCE & ASSOCIATES 2001 MARKET STREET, RM. 523 REDDING, CALIFORNIA 96001 (916) 244-9703	
SCALE: 1 INCH = 1/2 MILE	PLATE I